METHANE HEAT TRANSFER INVESTIGATION

8TH BI-MONTHLY TECHNICAL PROGRESS NARRATIVE
PERIOD OF PERFORMANCE: 14 APRIL - 14 JUNE 1984

CONTRACT NAS8-34977

Prepared for:
NASA/MSFC
Huntsville, Alabama 35812

14 JUNE 1984

Prepared by:

Ronald T. Cook Project Engineer

Ren Cook

Approved by:

F. M. Kirby

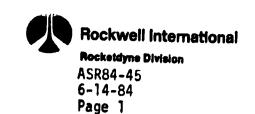
Program Manager Advanced Booster Propulsion Systems

(NABA-CA-171051) HUTHANE HEAT TRANSFER LaVESTEGATION Dimonthly Technical Progress Report, 14 Apr. - 14 Jun. 1984 (Rocketdyne) 4d p HC AUS/Hr AU1 CSCL 211

N84-29018

Unclas G3/48 19385

ROCKETDYNE DIVISION, ROCKWELL INTERNATIONAL CORPORATION 6633 Canoga Avenue; Canoga Park, California 91304



FOREWORD

This is a 12-month program being conducted for NASA-MSFC. The NASA-MSFC Program Monitor is Dale Blount. The major efforts of this program are being conducted by the Rocketdyne Engineering Aerothermal, and Materials Departments. Testing is being conducted at the Rockwell North American Aviation Operations (NAAO) Aerothermal Laboratory. The responsible Engineers in these areas are:

Ron Morinishi

Heat Transfer, Testing, Data Analysis

Dennis Lim

g.

3)

Task I Thrust Chamber Thermal Analysis

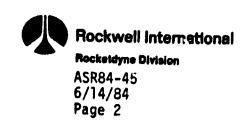
Frank Wimmer

Materials & Processes

Bob Scherer

Test (NAAO)

The Project Engineer is Ron Cook, Advanced Programs, and the Program Manager is Frank Kirby.



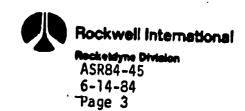
INTRODUCTION

This program is a 12-month experimental investigation to determine the coking thresholds and cooling capability (convective correlations) of methane. Economical exploitation of space in the future will require reusable, high-performance, liquid rocket booster engines. The high propellant bulk density and relatively high-performance LOX/hydrocarbon liquid engines look extremely attractive. LOX/methane is of particular interest because it has a higher chamber pressure cooling limit, higher specific impulse, higher coolant coking temperature, cleaner exhaust products, and lower potential for carbon deposition at low mixture ratio preburner operation than other hydrocarbon fuels.

Future high chamber pressure LOX/hydrocarbon booster engines will require copper-base alloy main combustion chamber coolant channels similar to the SSME to provide adequate cooling and reusable engine life. Therefore, it is of vital importance to evaluate the heat transfer characteristics and coking thresholds for LNG (94% methane) cooling, with a copper-base alloy material adjacent to the fuel coolant.

High-pressure methane cooling and coking characteristics have recently been evaluated at Rocketdyne using stainless-steel heated tubes at methane bulk temperatures and coolant wall temperatures typical of advanced engine operation except at lower heat fluxes as limited by the tube material. As expected, there was no coking observed. However, coking evaluations need be conducted with a copper-base surface exposed to the methane coolant at higher heat fluxes approaching those of future high chamber pressure engines.

This program consists of five working tasks and a reporting task.



TASK 1: Test Matrix Definition consists of (1) design and analysis of a 600K LOX/CH₄ Main Combustion Chamber (MCC) at 3000 psia chamber pressure and (2) definition of the test matrix to cover the ranges of methane coolant conditions described in the MCC design analysis. The MCC design will utilize a high strength copper base channel configuration coolant liner, typical of the Space Shuttle Main Engine (SSME). The test matrix will provide for definition of coking thresholds and convective cooling heat transfer correlations.

1

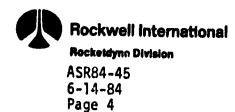
Control of the state of the sta

TASE 2: Design and Procurement of Test Sections consist of designing electrically heated tubular test specimens and procuring associated test specimen hardware. The test specimens will utilize a bimetallic tube assembly to allow testing at a heat flux of 50 Btu/in²-sec and 5000 psia CH₄ coolant pressure, which is typical of a 3000 psia chamber pressure MCC throat region coolant wall heat flux. The inner tube material will be copper to simulate any toking phenomena associated with the MCC liner material and surface conditions.

TASK 3: Preparation of Detail Test Plan consists of preparing a document that completely describes the test instrumentation, data acquisition, data correlation approach, heated tube specimen configuration control, and test procedures. The detailed test plan will include test section drawings, tube specimen operational maps, facility schematics, and data analysis processing procedures.

TASK 4: Heated Tube Testing will be conducted at the Rockwell North American Aviation Operations (NAAO) thermodynamics laboratory. Testing will be conducted to define the coking thresholds of methane at purities between 85% and 95% for LNG and near 100% pure methane. Coolant convective heat transfer characteristics will be evaluated at a purity between 94% and 100%.

TASK 5: Data Analysis and Correlation will be performed to define any coking thresholds and define convective cooling correlations for the complete range



of operating conditions applicable for a high chamber pressure MCC design. A number of convective heat transfer correlating formats will be satistically evaluated to obtain the best data-fit.

The program schedule, along with the work completed is shown in Table I.

DEV 5.75

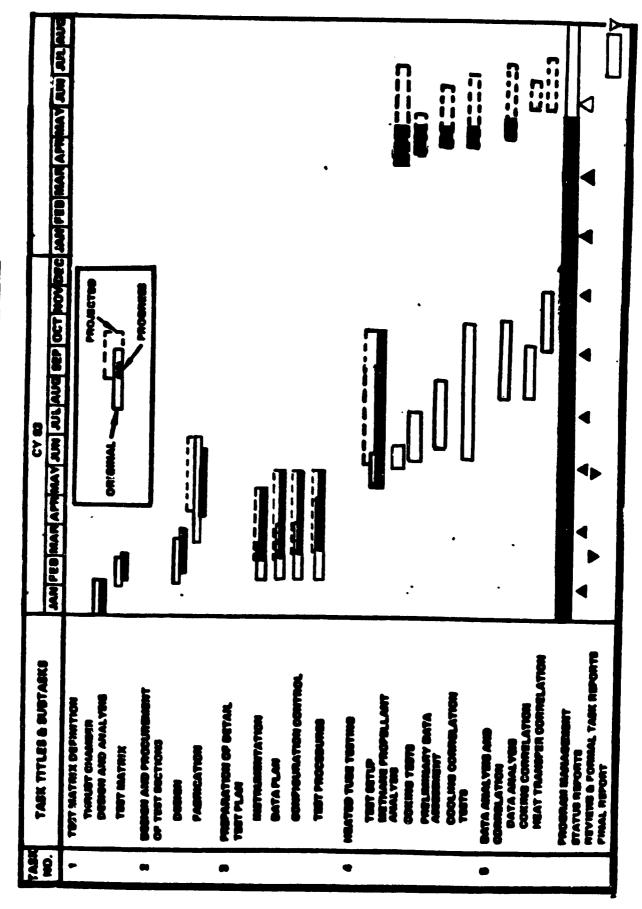
54 ~ 5 ~ 5

(ر

ORIGINAL FACE 15 OF POOR QUALITY

METHANE HEAT TRANSFER INVESTIGATION PROGRAM SCHEDULE (REVISED)

TABLE I



THE PROPERTY OF THE PROPERTY O

SUMMARY OF WORK ACCOMPLISHED

During this reporting period, the following work was accomplished:

- The first 500 gallon shipment of liquid methane was received on 17 May 1984 as part of an 11,000 gallon load being carried from Trussville, Alabama to Orange County.
- 2. Tests were run using a seven i.c. heated tube. The test facility performed well; no test delays were encountered. The instrumentation measurement accuracy was verified by the data reduction results. The heat balance between the wattmeter electrical measurement and the fluid enthalpy rise agreed within ±5% for the majority of the test points.
- 3. Analysis of the methane test data points is underway. Preliminary results show that the data is consistent and falls within the expected form of the Nusselt correlation. All data reduction and graphical output is being performed on the IBM Personal Computer.

人人が一个人の一人を見る一個の意味を見るというないない。 かからしょうかん かっしょうしん 大きのなる 古田子のかん は、一年のの一日本のでは、日本ののでは、

METHANE HEAT TRANSFER INVESTIGATION

DISCUSSION

TASK 4: HEATED TUBE TESTING

The second of th

Testing of the first 500 gallons of methane has been completed. These tests accomplished the following goals of the first phase of the rest plan: 1) verification of the bimetallic tube and test facility performance, 2) low heat flux range tests to provide heat transfer correlation data, and 3) heat transfer results which were within the predicted ±5% accuracy. The power reactors were driven up to 40 KWe (limit is 50 KWe) without the thermal runaway problem associated with the liquid nitrogen tests. All of these tests were performed on a single seven inch heated tube; no tube failures were encountered.

The methane chemical characteristics shown in Table 1 were provided by L. Hood Associates. Since the 500 gallons was delivered as part of a large shipment (approximately 10,000 gallons), it was assumed that the chemical make up was unchanged due to any boil-off during transit. However, a small sample of the methane was taken at the conclusion of the tests and will be analyzed.

The bimetallic tube temperature response to power input was well controlled, due to both the employment of fine tuning rheostats and the development of a test procedure which came from experience gained in the nitrogen tests. It was found that the desired tube temperature could be achieved more easily by first setting the desired power level (electrical current), then changing the fluid flow rate. Attempting to control the tube temperature by varying the power reactor inputs resulted in a "drifting" response. The general procedure for establishing a steady-state test point was to:

- 1. Start the fluid flow (about 2 gpm).
- 2. Turn on preheaters and activate power reactors.

1.4

3. Quickly ramp up the power, while maintaining a safe tube temperature by simultaneously increasing the flow rate.

P. C.

The state of the s

ではる方は

- 4. Once power is set, then achieve desired tube temperature by varying flow rate.
- 5. Allow system of reach steady-state for at least 25 seconds, then go to next test point.

This procedure required the coordination of two operators - one controlling the power reactors, and the other controlling the flow rate while monitoring the tube wall temperature.

The test was halted when over 25 gallons was flowed. This was indicated by a real-time integrator which is incorporated in the flowmeter counter. Note that although the run tank has a 33 gallon capacity, only about 25 gallons is usable due to the compressibility of the liquid. On a couple of occasions during the testing, the run tank was inadvertantly allowed to run dry; however, the automatic shutdown device (which monitors tube maximum temperature) acted quickly enough to prevent any tube damage. The device was set for a 1000°F limit.

There were no problems encountered in the instrumentation during the test period. The subsequent data analysis verified the accuracies of measurements. The wattmeter appeared to be performing up to its specified ±3% accuracy.

TASK 5: DATA ANALYSIS AND CORRELATION

The data analysis was performed on the IBM Personal Computer. A code called METHANE was written to simultaneously solve for the electrical heat generation and heat conduction balance in the bimetallic tube. The convective heat transfer coefficient is calculated at several axial positions along the tube. Fluid properties are accounted for by utilization of property correlations derived from the NBS tables. The METHANE code provides the pertinent dimensionless quantities such as Nusselt, Reynolds, Prandtl, and Stanton numbers. In addition, the temperature and viscosity property ratios (evaluated at bulk fluid and near wall conditions) are given at each axial location.

The results of the METHANE code were then transferred to a statistical sub-routine called NUCKLE which provides a best-fit correlation. The results from both programs were then graphically presented using the commercially available LOTUS 1-2-3 package.

The incorporation of all phases of the data reduction process into the PC allowed for quick and convenient analyses. Many of the test points were evaluated at the test site immediately after the run, providing valuable feedback for the test engineer.

The range of test conditions achieved during this period is shown in Table 2. The maximum heat flux of 25.8 Btu/sec-in² was achieved during the final run where the power reactors were outputting nearly 40 KWe. The tube wall was still a conservative 667°F, so a higher flux is possible on the seven inch tube. Limited runs were made at the higher flux levels due to the conservative test plan. Because of the thermal runaway problem encountered in the nitrogen tests, the initial methane tests were made by slowly increasing the power level. However, no indications of runaway were found.

The reduced data is shown in the Appendix section. Out of the 27 steady-state test points, only six had unacceptable heat balances --meaning that the measured

①

ASR84-45 6-14-84 Page 10

electrical power input to the tube did not match the measured enthalpy rise of the fluid. In most cases, the heat balance difference was within ±5%, which was the expected experimental accuracy. In the statistical fit process, only those data points with balances within ±8% were deemed acceptable. The unacceptable heat balances were found to be the result of unsteady test conditions at the time chosen for the data point. There was no correlation between power level and heat balance error as is shown in Fig. 1. Therefore, by taking more care in allowing the system to reach steady-state, acceptable results are achievable.

Since the standard correlation for convective heat transfer in pipe flow is the Dittus-Boelter equation, preliminary assessment of the reduced data was made by plotting Nu vs (Re^0.8 Pr^0.4) as is shown in Fig. 2. It is evident that the data is consistent; the data points fall along a nearly constant slope. Deviations from a constant slope are expected due to the varying fluid properties, and the large bulk fluid to tube wall temperature difference. This deviation in slope is evident in Fig. 3, which shows that as the fluid to wall temperature ratio decreases, the slope decreases from the Dittus-Boelter value of 0.023.

The best fit correlation for this preliminary form is,

$$Nu = 0.0163 \text{ Re}^{0.8} \text{ Pr}^{0.4}$$

A much better fit is found by adding the temperature ratio term to the Nusselt equation. This is shown in Fig. 4. The temperature ratio term accounts for the variation in fluid properties between the bulk fluid and near wall conditions. Important temperature related properties are viscosity, thermal conductivity, specific heat, and density. The preliminary best fit correlation for this form is,

Nu = 0.0215 Re^{0.8} Pr^{0.4}
$$(Tb/Tw)^{0.29}$$

Another form of the Nusselt equation separates the effect of the fluid viscosity from the temperature ratio term. Therefore, a viscosity ratio term is added, based on the bulk fluid and wall conditions. As shown in Fig. 5, there is not



ASR84-45 6-14-84 Page 11

an obvious increase in the data fit; however, a slight improvement may show up in the statistical fit. This has yet to be run.

An interesting comparison was made with similar methane tests run at Rocketdyne in 1979 by John Page. In the previous experiments, stainless tubes were electrically heated. The bimetallic tube was so designed to provide higher flux capabilities and better inner wall temperature calculation accuracy. The comparison is shown in Fig. 6. The previous data seems to give higher Nusselt numbers (hence, heat transfer coefficients) at the same Reynolds and Prandtl numbers (hence, flow conditions). The correlation that corresponds to this data is very close to the Dittus-Boelter equation, displaying a slope of 0.021.

A check was made to substantiate the fact that both data reduction calculations do indeed use the same methane properties (NBS). Also, a double check on the analytical solution to the bimetallic tube heat conduction ruation was performed in order to verify the METHANE data reduction accuracy. Is was done by comparison to a thermal model of the tube made on the Rocketdyne Thermal Analyzer Program (TAP). The results are shown in Fig. 7. It is evident that the analytical solution used in METHANE is indeed giving the correct tube wall temperatures. Therefore, at this time it is not known why the previous data is substantially different than the bimetallic tube test results. Further review of the data reduction procedure used by J. Page is underway.

Preparations are already underway for the next test series. A 3 inch tube has been installed in the test stand and a preliminary checkout is being performed. The next test series will be at higher heat flux and mass flux levels. The main focus of these tests will be to identify the conditions for incipient carbon coking. These tests will commence upon receipt of the next methane shipment, expected by the last week of June 1984.

WORK PLANNED

The following activities will be conducted during the next report period:

- 1. Preparations for the next series of tests will be complete. The tests will utilize a short 3 inch tube in order to the high heat fluxes. Incipient carbon coking will be investigated.
- The data analysis will be completed for the Nusselt correlation phase of the test plan. Also, a detailed evaluation of the previous methane tests (by J. Page in 1979) will be performed in order to make a positive comparison with the current test results.
- 3. Testing will commence upon the delivery of methane, expected by 30 June 1984.

Table 1. Methane chemical composition

COMPONENT	MOLE %
Oxygen	0.020
Nitrogen	0.290
Carbon Dioxide	0.000
Methane	92.470
Ethane	6.042
Propane	0.929
I-Butane	0.113
N-Butane	0.099
I-Pertane	0.000
N-Pentane	0.000
Hexanes	0.000

Excerpt from the Chromatographic analysis report prepared by Southern Natural Gas Co., Measurement Dept, Birmingham, Alabama on 3/16/84.

T

50 meter 6 4 - 8 2

Table 2. Range of test conditions achieved in first test series.

Total Number of Tests	14			
Total Number of Data Points	27			
Nusselt Number	1067	to	3467	
Reynolds Number	8.2 E5	to	3.8 E6	
Heat Flux	1.6	to	25.B	Btu/s-in2
Mass Flux	23.9	to	68.8	lbm/s-in2
Inlet Fluid Temperature	-139	to	-36	F
Dutlet Fluid Temperature	-118	to	23	F
Inlet Fluid Pressure	3914	to	4966	PSia
Fluid Velocity	181	to	781	ft/s

The second of th

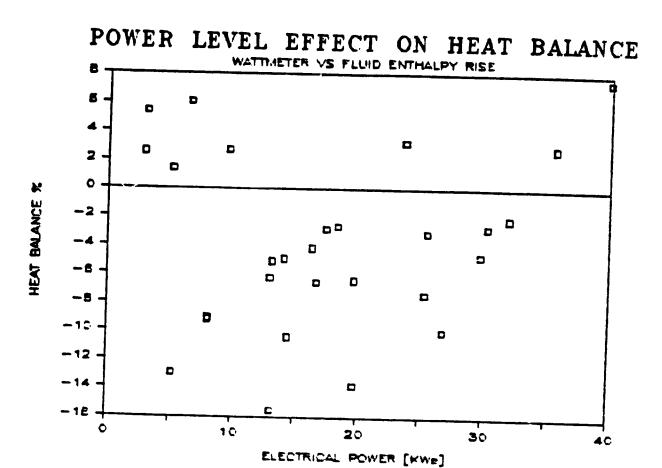
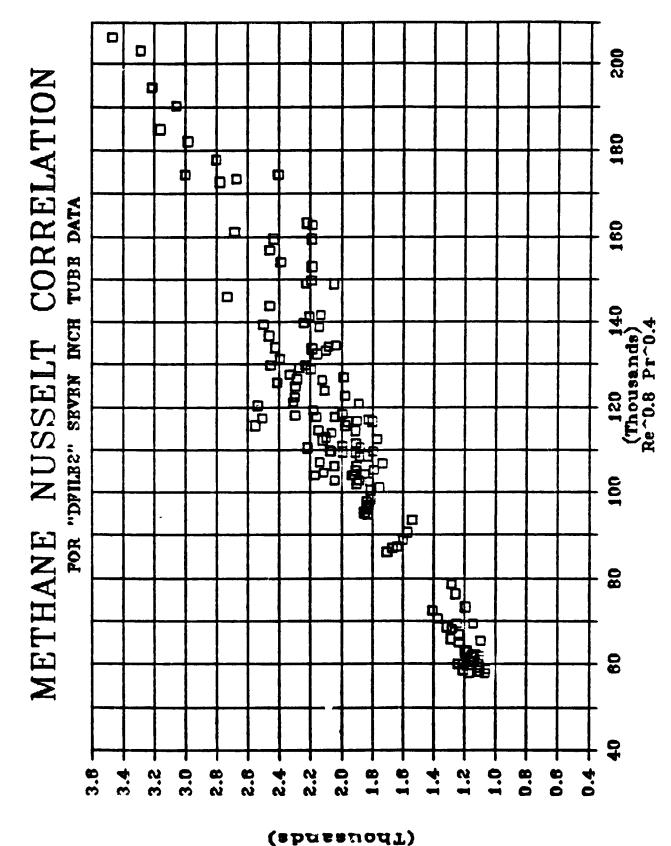


Figure 1. Power Level Effect on Heat Balance

THE THE PROPERTY OF THE PROPER

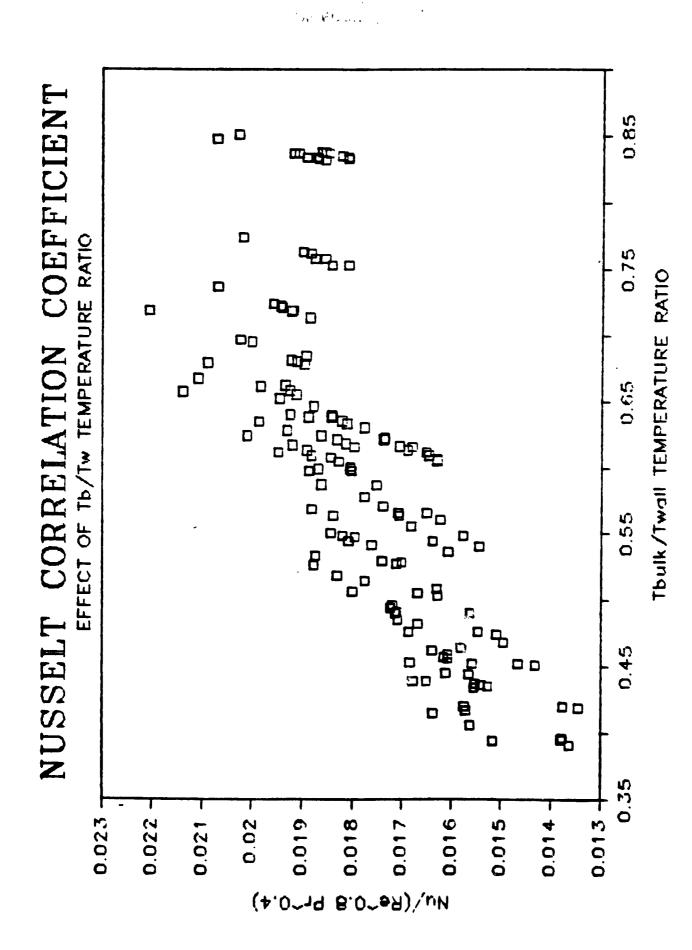
(+)



NUSSELT NUMBER

TO THE PROPERTY OF THE PARTY OF

Dittus-Boelter Form of Nusselt Correlation 7: Figure



o come of the state of the stat

Figure 3. Nusselt Coefficient Dependence on Temperature Ratio

T

OF POUR QUALITY

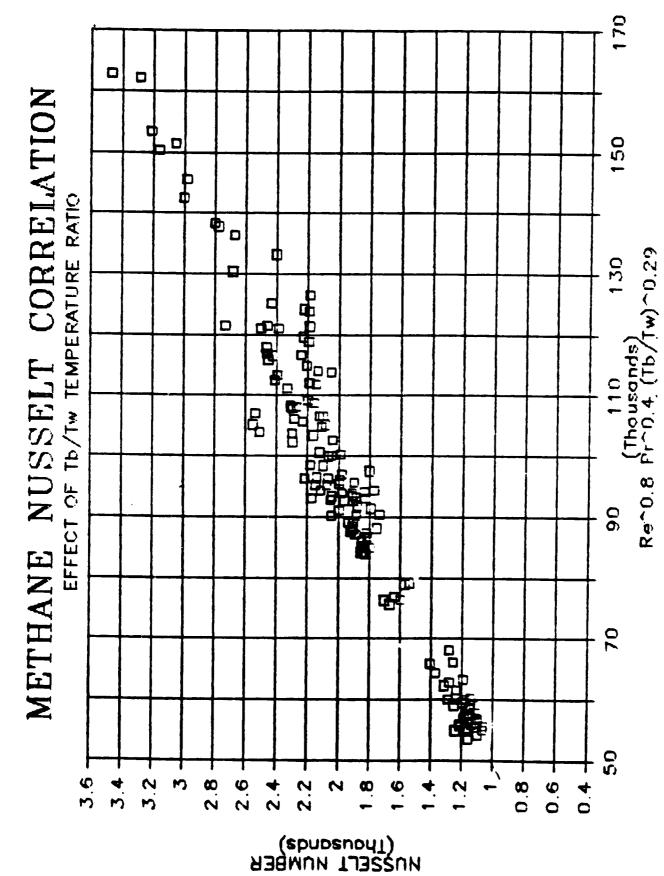
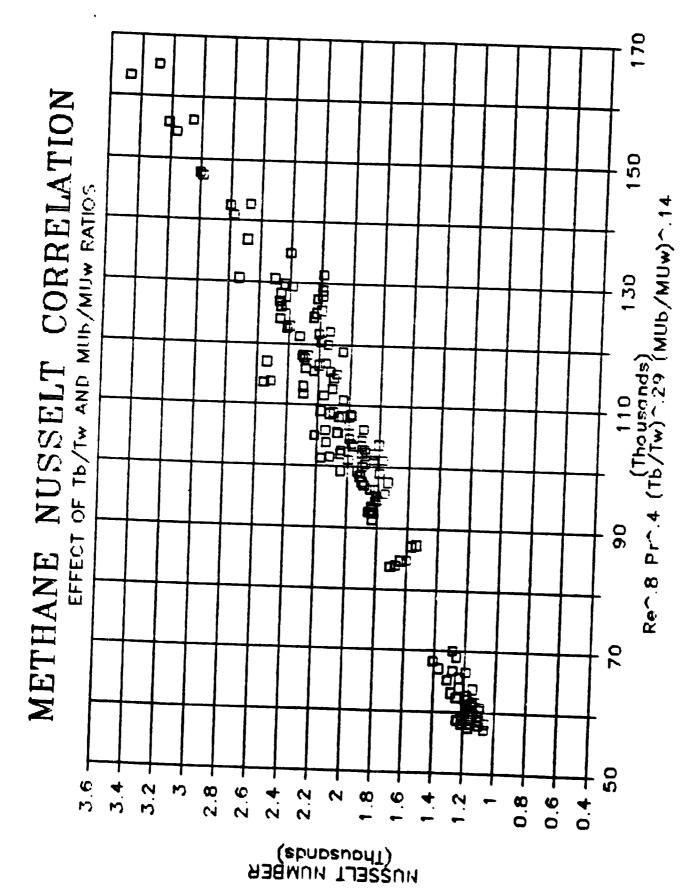


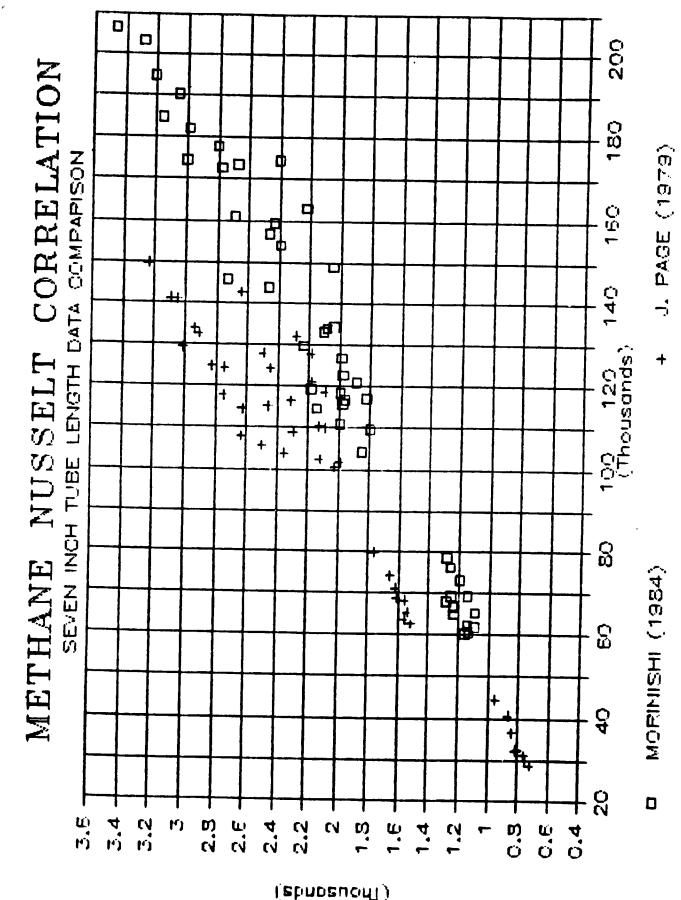
Figure 4. Nusselt Correlation with Temperature Ratio Term



The second of th

Figure 5. Nusselt Correlation with Temperature Ratio and Viscosity Ratio Terms

•



flusselt flo.

°٥̈

TO SEE THE SECOND SECON

Comparison of Present Results with Previous Rocketdyne Methane Tests

Figure 6.

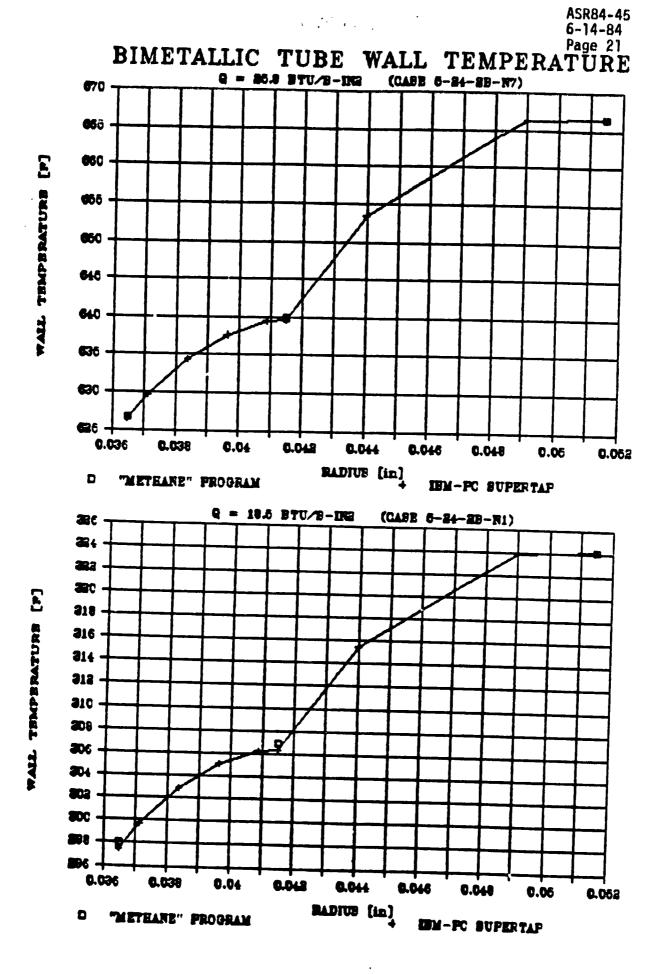


Figure 7. Comparison of the Bimetallic Tube Heat Conduction Solutions

D

4

(+)

ASR84-45 6-14-84 Page 22

APPENDIX

REDUCED DATA

(

-

- 🕴 .

, ÷

METHANE HEAT TRANSFER INVESTIGATION

```
# OF TC = 7
              Vol Flow = 2.37 [GFM] Mass Flow = .1040[1b/s] Mass Flux = 24.84[1b/s-in2]
              WALL X/ID OUTER INTERF INNER FLUID ADIAB. FLUID HEAT & TRANSFER
           NALL X/ID GUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER LOC.

X[in] WALL WALL WALL BULK NALL T PRESS FLUX COEFFICIENT T[F] T[F] T[F] T[F] T[F] T[F] [psia] [Btu/s-in+2]

.14 1.9 12.4 11.1 10.3 -59.6 -58.8 4860.6 1.627 .23550E-01

.97 13.3 19.1 17.8 17.0 -60.7 -59.8 4852.5 1.650 .21467E-01

1.91 26.2 28.1 2e.7 26.0 -55.0 -54.1 4937.2 1.680 .20979E-01

4.16 57.0 34.1 32.7 31.9 -47.6 -46.7 4817.5 1.699 .21617E-01

5.02 68.8 43.3 41.9 41.1 -41.6 -40.6 4801.5 1.730 .21171E-01

6.10 83.6 47.0 45.6 44.7 -37.0 -36.0 4789.5 1.741 .21560E-01

6.84 93.7 53.7 52.2 51.4 -33.4 -32.5 4780.2 1.764 .21007E-01
WALL TURE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT LOC. SEG DL CU MONEL CU MONEL CU MONEL O GEN LOSS X[1n] [in] [mOhns/in] [volt/in] [amps] [Ptu/s-in] [Ptu/s-in] .14 .555 .50 11.32 .43 868. 38. .36 .02 .37 .00 .97 .895 .51 11.33 .44 867. 39. .36 .02 .37 .00 .1.91 1.595 .52 11.34 .45 867. 40. .37 .02 .39 .00 .4.16 1.555 .52 11.34 .45 866. 40. .37 .02 .39 .00 .4.16 1.555 .52 11.34 .45 866. 40. .37 .02 .39 .00 .90 .970 .53 11.35 .46 865. 41. .38 .02 .40 .00 .10 .910 .54 11.35 .47 865. 41. .38 .02 .40 .00 .66
       WALL FLUID REYNCLDS FRANDTL TEUIK/ MUBUIK/ NUSSELT STANTON
LOC. VEL. NUMBER NUMBER TWAII MUWAII NUMBER NUMBER
           X[in] [ft/s]
.14 181.4 .8173E+06 1.209 .851 1.30 .1173E+04 .1187E-02 .97 181.0 .8141E+06 1.211 .837 1.34 .1067E+04 .1082E-02 1.91 183 5 .8311E+06 1.210 .833 1.36 .1061E+04 .1055E-02 4.16 186.7 .8540E+06 1.203 .838 1.36 .1114E+04 .1084E-02 5.02 189.5 .8735E+06 1.197 .835 1.37 .1107E+04 .1059E-02 6.10 191.6 .8883E+05 1.195 .838 1.36 .1142E+04 .1076E-02 6.84 193.3 .9005E+06 1.192 .834 1.38 .1125E+04 .1046E-02
WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL LOC. TEMP. PRESS VISCOSITY CONDUCTIVITY
                                                                                                                                                                          SPECIFIC DENSITY
LOC. TEMP. PRESS VISCOSITY CONDUCTIVITY HEAT X[in] [F] [psia] [Btu/lb] [lb/ft-e] [Btu/s-ft] [Btu/lb-R] [lb/ft3] .14 -59.6 4860.6 304.624 .2663E-04 .17590E-04 .7984 19.721 .97 -60.7 4852.5 303.732 .2673E-04 .17629E-04 .7985 19.760 1.91 -55.0 4837.2 308.419 .2618E-04 .17321E-04 .8003 19.497 4.16 -47.6 4817.5 314.488 .2548E-04 .16999E-04 .8028 19.156 5.02 -41.6 4801.5 519.453 .2492E-04 .16757E-04 .8049 18.878 10 -37.0 4789.5 323.230 .2450E-04 .16537E-04 .8065 18.667 34 -33.4 4780.2 326.160 .2417E-04 .16376E-04 .8078 18.503
                                                                           VISCOSITY CONDUCTIVITY HEAT
CALC. CHECK: Wattmeter Qe = 2.88[kw] Sensible Qs = 2.80[kw] Qerr = 2.58% Meas. V = .100 [volts] Calc. V = 3.173 [volts] Verr = 0.00 (NO CATA) Meas. I = 0.00 [amps] Calc. I = 906.1 [amps] Ierr = 96.85% Meas. Tout = -25.5 [F] Calc. Tout = -32.1 [F] Terr = 6.6 &F]
```

METHANE HEAT TRANSFER INVESTIGATION

= CASE = 5-17-3C TIME = 14:58:29 TUBE L = 7.02 (in) # OF TC = 7 Vol Flow = 2.36 [GPM] Mass Flow = .0999[1b/s] Mass Flux = 23.88[1b/s-in2] WALL TUBE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT WALL TUBE RESISTANCE CU MONEL CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [mOhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] .14 .555 .52 11.34 .45 870. 40. .37 .02 .39 .00 .97 .885 .53 11.35 .46 870. 41. .38 .02 .40 .00 .1.91 1.595 .54 11.35 .47 869. 41. .39 .02 .40 .00 .416 1.555 .55 11.36 .47 868. 42. .39 .02 .41 .00 .92 .970 .56 11.36 .48 868. 42. .39 .02 .41 .00 .10 .910 .56 11.36 .49 867. 43. .40 .02 .42 .00 .6.84 .550 .57 11.37 .49 867. 43. .40 .02 .42 .00 .14 180.5 .8297E+06 1.201 .848 1.33 .1210E+04 .1214E-02 .97 180.2 .8271E+06 1.202 .834 1.37 .1103E+04 .1109E-02 1.91 183.0 .8464E+06 1.194 .832 1.38 .1099E+04 .1087E-02 4.16 186.6 .8724E+06 1.191 .837 1.37 .1162E+04 .1118E-02 5.02 189.7 .8944E+06 1.181 .833 1.38 .1151E+04 .1090E-02 6.10 192.1 .9117E+06 1.180 .837 1.37 .1193E+04 .1109E-02 6.84 194.1 .9256E+06 1.170 .834 1.38 .1181E+04 .1090E-02 WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY VISCOSITY CONDUCTIVITY HEAT SPECIFIC DENSITY DENSITY DENSITY DENSITY DENSITY HEAT SPECIFIC DENSITY DENSITY DENSITY DENSITY HEAT SPECIFIC DENSITY DENSITY HEAT SPECIFIC DENS CALC. CHECK: Wattmeter Ge = 3.03[kw] Sensible Gs = 2.86[kw] Gerr = 5.45%

Meas. V = .100 [volts] Calc. V = 3.323 [volts] Verr messess%

Meas. I = 444444 [amps] Calc. I = 910 2 [amps] Ierr = 96.99%

Meas. Tout = -8.8 [F] Calc. Tout = -14.3 [F] Terr = 5.5 [F]

METHANE HEAT TRANSFER INVESTIGATION

4

The second secon

The state of the

D

```
CASE = 5-17-3D
                                     TIME = 15:00:51
                                                               TUBE L = 7.02 (in) # OF TC =
         (Qabse = 6.53 [KWe] | I =1212.4 [amps] | V = 5.382 [volts] | R = 4.44 [mDhms]
         Tu/s= -36.1 [F] Td/s= 33.9 [F] Pin =4843.0 [psia] Pout = 4600.0 [psia] Tin = -37.0 [F] Tout = 34.3 [F] Hin= 323.3 Hout = 381.2 [Btu/lb]
          Vol Flow = 2.41 [GPM]
                                             Mass Flow = .1002[1b/s] Mass Flux = 23.94[1b/s-in2]
         WALL X/ID OUTER INTERF INNER FLUID ADIAB. FLUID
                                                                                          HEAT
         LOC.
                                                                                                    h TRANSFER
        WALL WALL BULK WALL T PRESS FLUX
                            WALL
         WALL
                 TUBE
                             RESISTANCE VOLTAGE
                                                            CURRENT
                                                                            HEAT GEN.
        LOC. SEG DL CU MONEL
                                                                                             TOTAL
                                                                                                           HEAT
                                                           CU MONEL CU MONEL Q GEN LOSS
       X[in] [in] [mDhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in]
                          Emulhms/in] [volt/in] [amps] LBTU/s-in] LBTU/s-i

.61 11.39 .70 1151.62.76 .04 .81

.63 11.41 .73 1149.64.79 .04 .83

.65 11.42 .75 1147.66.82 .05 .86

.67 11.43 .77 1145.67.83 .05 .88

.70 11.44 .80 1143.69.86 .05 .91

.71 11.45 .81 1142.71.88 .05 .93

.72 11.46 .82 1141.72.89 .06 .95
        .14 .555
.97 .885
        1.91 1.595
        4.16 1.555
                                                                                                            .00
       92 .970
2.10 .910
4.84 .550
                                                                                                            .00
                                                                                                            .00
                                                                                                            .00
                                                                                                            .00
      WALL FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON
      LOC. VEL.
X[in] [ft/s]
                          NUMBER NUMBER Twall MUwall
                                                                              NUMBER NUMBER
     WALL FLUID FLUID ENTHALPY DYNAMIC
                                                                  THERMAL
       LOC. TEMP. PRESS
                                                                                  SPECIFIC DENSITY
     LUC. TEMP. PRESS VISCOSITY CONDUCTIVITY NEAT X[in] [F] [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3] .14 -37.0 4739.7 323.253 .2450E-04 .16512E-04 .8086 18.611 .97 -32.5 4730.9 326.958 .2409E-04 .16389E-04 .8102 18.407 .97 -19.6 4714.3 337.686 .2293E-04 .15803E-04 .8142 17.827 .16 -2.6 4692.6 351.764 .2147E-04 .15106E-04 .8192 17.075 .02 11.4 4674.5 363.464 .2033E-04 .14477E-04 .828 16.458 .10 22.3 4660.5 372.552 .1950E-04 .14002E-04 .8249 15.986 .31.0 4649.4 379.782 .1887E-04 .13630E-04 .8262 15.616
                                                VISCOSITY CONDUCTIVITY HEAT
     CALC. CHECK: Wattmeter De = 6.53[kw] Sensible Os = 6.13[kw] Gerr = 6.09%
Meas. V = 5.330 [volts] Calc. V = 5.382 [volts] Verr = .968%

Meas. I = 1224.2 [amps] Calc. I = 1212.4 [amps] lerr = .96%

Meas. Tout = 32.7 [F] Calc. Tout = 34.3 [F] Terr = 1.6 [F]
```

OF POOR CARACT

METHANE HEAT TRANSFER INVESTIGATION

```
CASE = 5-18-1A TIME = 11:28:55 TUBE L = 7.02 [in] # OF TC = 7
                   Vol Flow = 2.48 [GPM] Mass Flow = .1098[15/s] Mass Flux = 26.23[15/s-in2]
               WALL X/ID DUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER LOC. WALL WALL BULK WALL T PRESS FLUX COEFFICIENT T[F] T[F] T[F] T[F] T[F] T[F] [psia] [Btu/s-in**2] .14 1.9 53.5 51.2 49.9 -65.2 -64.3 4637.1 2.809 .24613E-01 .91 26.2 87.6 85.0 83.7 -50.6 -49.4 4627.1 2.902 .22873E-01 4.16 57.0 96.9 94.3 92.9 -38.4 -37.3 4585.7 3.036 .23325E-01 5.02 68.8 113.1 110.4 108.9 -28.7 -27.6 4566.6 3.119 .22851E-01 6.10 83.6 119.7 116.9 115.5 -21.3 -20.2 4552.1 3.153 .23249E-01 6.84 93.7 135.0 132.1 130.6 -15.6 -14.4 4540.6 3.232 .22290E-01
WALL TUBE RESISTANCE CU MONEL 
WALL FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUwall NUMBER NUMBER
WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY VISCOSITY CONDUCTIVITY HEAT

[F] [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3]

.14 -65.2 4637.1 299.842 .2717E-04 .17861E-04 .8056 19.752

.97 -60.4 4627.1 303.883 .2670E-04 .1762BE-04 .8072 19.524

1.91 -50.6 4609.1 311.968 .2576E-04 .17135E-04 .8104 19.072

4.16 -38.4 4585.7 322.157 .2462E-04 .16575E-04 .8319 18.501

5.02 -28.7 4566.6 330.247 .2374E-04 .16203E-04 .8363 18.047

.10 -21.3 4552.1 336.401 .2309E-04 .15908E-04 .8394 17.703

.84 -15.6 4540.6 341.253 .2258E-04 .15624E-04 .8416 17.431
CALC. CHECK: Wattmeter Qe = 5.15[kw] Sensible Qs = 5.08[kw] Qerr = 1.40%

Meas. V = 4.423 [volts] Calc. V = 4.489 [volts] Verr = 1.501%

Meas. I = 1164.5 [amps] Calc. I = 1147.2 [amps] Jerr = 1.48%

Meas. Tout = -14.1 [F] Calc. Tout = -13.4 [F] Terr = .8 [F]
```

)

METHANE HEAT TRANSFER INVESTIGATION

. . . i — ::tY

. .

```
CASE = 5-18-18
                                                                               TIME = 11:30:52 TUBE L = 7.02 [in] # OF TC = 7
          Q_0bse = 9.65 [KWe] I =1383.9 [amps] V = 6.973 [volts] R = 5.04 [mDhms] T u/s= -61.4 [F] T d/s= 37.1 [F] Pin =4732.0 [psia] Pout = 4523.0 [psia] T in = -62.3 [F] Tout = 38.4 [F] H in= 302.3 H out = 384.3 [Btu/lb]
              WALL X/ID DUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER
     WALL TUBE RESISTANCE CU MONEL 
. WALL FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON
        LOC. VEL. NUMBER NUMBER Twall MUWall NUMBER NUMBER
        X[in] [ft/s]
WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY CONDUCTIVITY HEAT VISCOSITY CONDUCTIVITY HEAT

X[in] [F] [psie] [Btu/1b] [1b/ft-s] [Btu/s-ft] [Btu/1b-R] [1b/ft3]

.14 -59.1 4616.3 304.936 .2657E-04 .17566E-04 .8079 19.457

.97 -49.8 4605.5 312.584 .2569E-04 .17082E-04 .8108 19.035

1.91 -32.8 4585.8 326.757 .2412E-04 .16375E-04 .8338 18.256

4.16 -10.5 4559.7 345.432 .2214E-04 .15483E-04 .8419 17.238

5.02 8.1 4537.6 361.087 .2059E-04 .14631E-04 .8466 16.396

7.10 22.6 4520.2 373.209 .1948E-04 .13990E-04 .8495 15.756

.84 34.0 4506.2 382.845 .1866E-04 .13506E-04 .8497 15.255
          CALC. CHECK: Wattmeter Qe = 9.65[kw] Sensible Qs = 9.39[kw] Qerr = 2.70%
```

o a la company of the same of

ORIGINAL NEWS OF POOR CUALITY

METHANE HEAT TRANSFER INVESTIGATION

The second of th

CASE = 5-18-2C TIME = 13:54:40 TUBE L = 7.02 [in] # OF TC = 7 (Qabse =14.45 [KWe] I =1810.3 [amps] V = 7.982 [volts] R = 4.41 [mDhms] T u/s=-130.9 [F] T d/s=-42.0 [F] Pin =3914.0 [psia] Pout = 3345.0 [psia] T in =-133.1 [F] T out = -53.1 [F] H in = 241.4 H out = 319.0 [Btu/lb] Vol Flow = 3.93 [GPM] Mass Flow = .1947[1b/s] Mass Flux = 46.53[1b/s-in2] WALL X/ID DUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER WALL TUBE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT LOC. SEG DL CU MONEL CU MONEL Q GEN LOSS LOC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [mOhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] .14 .555 .56 11.37 .97 1725. B5. 1.59 .08 1.67 .00 .97 .885 .60 11.40 1.03 1720. 90. 1.68 .09 1.77 .00 1.91 1.595 .65 11.42 1.11 1713. 97. 1.80 .10 1.90 .00 4.16 1.555 .65 11.43 1.12 1713. 98. 1.81 .10 1.91 .00 .00 .10 .90 .71 11.46 1.21 1704. 106. 1.96 .12 2.08 .00 .10 .910 .74 11.48 1.26 1701. 109. 2.02 .13 2.15 .00 6.84 .550 .76 11.49 1.30 1698. 113. 2.08 .14 2.22 .00 WALL FLUID REYNOLDS PRANDTL Tbulk/ MUbulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUwall NUMBER NUMBER X[in] [ft/s] .14 305.3 .1254E+07 1.317 .613 2.14 .1500E+04 .9084E-03 .97 311.0 .1311E+07 1.297 .590 2.19 .1443E+04 .8486E-03 1.91 322.3 .1354E+07 1.345 .569 2.18 .1450E+04 .7959E-03 4.16 338.9 .1483E+07 1.328 .593 2.01 .1626E+04 .8261E-03 5.02 354.6 .1598E+07 1.335 .563 1.89 .1602E+04 .7504E-03 6.10 368.4 .1696E+07 1.346 .560 1.79 .1667E+04 .7303E-03 6.84 380.4 .1777E+07 1.356 .554 1.71 .1707E+04 .7087E-03 WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY LOC. TEMP. PRESS VISCOSITY CONDUCTIVITY HEAT

WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY VISCOSITY CONDUCTIVITY HEAT

X[in] [F] [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3]
.14 -130.3 3589.3 243.782 3250E-04 .20632E-04 .8362 21.947
.97 -122.7 3561.2 250.197 .3109E-04 .2013BE-04 .8403 21.543
1.91 -108.9 3509.7 261.994 .3009E-04 .19016E-04 .8499 20.786
4.16 -91.1 3441.2 277.450 .2749E-04 .17953E-04 .8672 19.767
5.02 -76.6 3383.4 290.319 .2550E-04 .16900E-04 .8850 18.895
10 -65.4 3337.5 300.557 .2404E-04 .16091E-04 .9011 18.187
84 -56.4 33300.4 308.737 .2293E-04 .15461E-04 .9139 17.612

CALC. CHECK: Wattmeter Qe =14.45[kw] Sensible Qs =15.95[kw] Qerr = .400%
Heas. I =1817.5 [amps] Calc. V = 7.982 [volts] Verr = .400%
Heas. Tout = -45.2 [F] Calc. Tout = -53.1 [F] Terr = 7.9 [F]

The state of the s

```
METHANE HEAT TRANSFER INVESTIGATION
     CASE = 5-18-3A TIME = 14:36:34 TUBE L = 7.00 [in]
                                                                                                                                                                                                     # OF TC = 7
  WALL TUBE RESISTANCE CU MONEL 
  WALL FLUID REYNOLDS PRANDTL Tbulk/ MUbulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUwall NUMBER NUMBER NUMBER
  X[in] [ft/s]
CALC. CHECK: Wattmeter De = 8.05[kw] Sensible Qs = 8.79[kw] Derr = 9.16%
Meas. V = 5.239 [volts] Calc. V = 5.312 [volts] Verr = 1.392% Meas. I =1536.5 [amps] Calc. I =1515.3 [amps] lerr = 1.38% Meas. Tout = -64.2 [F] Calc. Tout = -68.3 [F] Terr = 4.1 [F]
```

Contract of the second

The state of the s

...

للمنافعية المراجعة الماسية

METHANE HEAT TRANSFER INVESTIGATION OF POOR QUALITY CASE = 5-18-3A TIME = 14:36:42 TUBE L = 7.02 [in] # OF TC = 7 Qabse = 8.08 [KWe] I =1513.7 [amps] V = 5.334 [volts] R = 3.52 [mDhms] T u/s=-113.1 [F] T d/s: -61.4 [F] Pin =4439.0 [psia] Pout = 3848.0 [psia] T in =-115.4 [F] Tout = -68.3 [F] H in= 257.3 H out = 300.5 [Btu/lb] Vol Flow = 3.99 [GPM] Mass Flow = .1934[1b/s] Mass Flux = 46.21[1b/s-in2] WALL X/ID DUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER LOC. WALL WALL WALL BULK WALL T PRESS FLUX COEFFICIENT WALL TUBE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT LOC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN LOSS

LOC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [mDhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] .14 .555 .49 11.33 .70 1451.62.97 .04 1.01 .00 .97 .885 .50 11.33 .72 1450.64.99 .04 1.03 .00 1.91 1.595 .52 11.34 .75 1448.66.1.03 .05 1.08 .00 4.16 1.555 .52 11.34 .75 1447.66.1.03 .05 1.08 .00 .00 .02 .970 .55 11.36 .79 1444.69.1.08 .05 1.13 .00 .10 .910 .55 11.37 .80 1443.70.1.10 .05 1.15 .00 6.84 .550 .57 11.37 .82 1442.72.1.11 .06 1.17 .00

WALL FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUWall NUMBER NUMBER X[in] [ft/s]

WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY LOC. TEMP. PRESS VISCOSITY CONDUCTIVITY HEAT LUC. TEMP. PRESS VISCOSITY CONDUCTIVITY HEAT X[in] [F] [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3] .14 -113.7 4113.9 258.815 .3048E-04 .20662E-04 .8226 21.548 .97 -109.0 4087.5 262.653 .3179E-04 .19851E-04 .8250 21.306 1.91 -100.9 4039.9 269.452 .3086E-04 .19706E-04 .8300 20.872 4.16 -90.4 3978.2 278.226 .2963E-04 .19214E-04 .8381 20.301 5.02 -81.9 3927.4 285.406 .2852E-04 .18622E-04 .8457 19.826 .10 -75.4 3888.7 290.946 .2767E-04 .18149E-04 .8521 19.456 .84 -70.2 3858.1 295.316 .2700E-04 .17792E-04 .8576 19.162

CALC. CHECK: Wattmeter Qe = 8.08[kw] Sensible Qs = 8.81[kw] Qerr = 9.10% Meas. V = 5.301 [volts] Calc. V = 5.334 [volts] Verr = .629% Meas. I =1523.3 [amps] Calc. I =1513.7 [amps] Ierr = .63% Heas. Tout = -64.2 [F] Calc. Tout = -68.3 [F] Terr = 4.1 [F]

'n,

- Ut Will Willy House the Character of the

ជ

=

25 A B B

```
METHANE HEAT TRANSFER INVESTIGATION
                                                                                                 OF the most of the
     CASE = 5-18-38
                                TIME = 14:38:16 TUBE L = 7.00 [in] # OF TC =
   (Qabse =13.18 [KWe] I =1767.3 [amps] V = 7.455 [volts] R = 4.22 [mOhms]
    Tu/s=-109.8 [F] Td/s= -30.3 [F] Pin =4380.0 [psia] Pout = 3746.0 [psia] Tin =-112.2 [F] Tout = -37.3 [F] Hin= 259.9 Hout = 327.4 [Btu/1b]
    Vol Flow = 4.05 [GPM] Mass Flow = .1946[1b/s] Mass Flux = 46.48[1b/s-in2]
   WALL X/ID DUTER INTERF INNER FLUID ADIAB. FLUID HEAT
                                                                                                    h TRANSFER
   LOC.
  WALL
                                WALL WALL BULK WALL T PRESS FLUX COEFFICIENT
  WALL
            TUBE RESISTANCE VOLTAGE CURRENT
  LOC. SEG DL CU MONEL
                                                                            HEAT GEN. TOTAL
                                                                                                            HEAT
 LUC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [mDhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] .14 .555 .56 11.37 .94 1685. B2. 1.49 .07 1.57 .00 .97 .885 .58 11.38 .98 1682. B6. 1.55 .08 1.63 .00 1.91 1.595 .63 11.41 1.05 1676. 92. 1.66 .09 1.75 .00 4.16 1.555 .62 11.41 1.04 1676. 91. 1.65 .09 1.74 .00 .92 .970 .68 11.44 1.13 1669. 98. 1.78 .11 1.89 .00 .10 .910 .70 11.45 1.17 1666. 102. 1.84 .11 1.95 .00 6.84 .530 .72 11.47 1.19 1663. 104. 1.88 .12 2.00 .00
                                                          CU MONEL CU MONEL Q GEN LOSS
  WALL FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON
  LOC. VEL. NUMBER NUMBER Twall MUwall
                                                                              NUMBER NUMBER
  X[in] [ft/s]
WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL
                                                                                   SPECIFIC DENSITY
 LOC. TEMP. PRESS
LDC. TEMP. PRESS VISCOSITY CONDUCTIVITY HEAT X[in] [F] [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3] .14 -109.5 4046.7 262.176 .3184E-04 .19862E-04 .8265 21.295 .97 -102.3 4018.2 268.150 .3103E-04 .19750E-04 .8303 20.925 1.91 -89.4 3966.0 279.048 .2948E-04 .19108E-04 .8391 20.241 4.16 -72.7 3897.2 293.201 .2744E-04 .17989E-04 .8533 19.333 5.02 -59.2 3839.6 304.875 .2581E-04 .17129E-04 .8662 18.573 10 -48.5 3794.3 314.121 .2457E-04 .16464E-04 .8757 17.967 .84 -40.3 3758.4 321.436 .2362E-04 .15959E-04 .8827 17.483
                                               VISCOSITY CONDUCTIVITY HEAT
 CALC. CHECK: Wattmeter De =13.18[kw] Sensible Os =13.84[kw] Qerr = 5.06%
 Meas. V = 7.453 [volts] Calc. V = 7.455 [volts] Verr = .031% Meas. I =1767.9 [amps] Calc. I =1767.3 [amps] lerr = .03% Meas. Tout = -33.6 [F] Calc. Tout = -37.3 [F] Terr = 3.6 [F]
```

The second of th

THE WALL STREET AND STREET AND STREET AND STREET AND STREET ASSESSED TO STREET AND ASSESSED AND STREET AND ASSESSED ASSESSED

一年 日本の日本日本

è

上本人が出来」を一下

U

```
OF POOR QUALITY
                                              METHANE HEAT TRANSFER INVESTIGATION
        CASE = 5-18-3C    TIME = 14:39:19    TUBE L = 7.02 [in] # OF TC = 7
Vol Flow = 4.09 [GPM] Mass Flow = .1959[1b/s] Mass Flux = 46.80[1b/s-in2]
      WALL TUBE RESISTANCE CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [mOhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] [Btu/s-in] .14 .555 .60 11.39 1.05 1771. 92. 1.77 .09 1.86 .00 .97 .B85 .63 11.41 1.11 1766. 97. 1.86 .10 1.96 .00 1.91 1.595 .69 11.45 1.22 1757. 107. 2.03 .12 2.15 .00 4.16 1.555 .69 11.45 1.21 1758. 106. 2.02 .12 2.14 .00 .92 .979 .77 11.50 1.34 1747. 117. 2.22 .15 2.37 .00 .10 .910 .81 11.52 1.41 1741. 122. 2.33 .16 2.49 .00 6.84 .550 .84 11.54 1.46 1737. 127. 2.41 .18 2.58 .00
   WALL FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUwall NUMBER NUMBER X[in][ft/s]
 NALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY VISCOSITY CONDUCTIVITY HEAT
X[in] [F] [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3]
.14 -109.0 3959.8 262.452 .3165E-04 .19770E-04 .8298 21.197
.97 -100.5 3930.0 269.548 .3056E-04 .19549E-04 .8348 20.757
1.91 -84.9 3874.8 282.743 .2861E-04 .18659E-04 .8464 19.925
4.16 -64.8 3801.0 299.961 .2619E-04 .17332E-04 .8648 18.818
5.02 -48.4 3738.2 314.381 .2428E-04 .16320E-04 .8906 17.874
10 -35.4 3687.7 326.029 .2284E-04 .15527E-04 .8911 17.109
84 -25.0 3646.6 335.433 .2173E-04 .14956E-04 .8980 16.491
```

بالكتر

٧. و

CALC. CHECK: Wattmeter De =16.37[km] Sensible Os =17.05[km] Gerr = 4.14% Meas. V = 8.777 [volts] Calc. V = 8.788 [volts] Verr = .117% Meas. I = 1865.6 [amps] Calc. I = 1863.4 [amps] Ierr = .12% Meas. Tout = -17.3 [F] Calc. Tout = -21.0 [F] Terr = 3.7 [F]

to a series of the series of t

Car Carlie James

METHANE HEAT TRANSFER INVESTIGATION

...

一本を記しているというできるとは、それのできないというとしていると

. Ť.

```
CASE = 5-18-4A
                                      TIME = 15:38:00 TUBE L = 7.02 [in] # OF TC = 7
       Vol Flow = 4.53 [GPM] Mass Flow = .2199[lb/s] Mass Flux = 52.53[lb/s-in2]
     WALL TUBE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT
LOC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN LOSS
     LUC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [mOhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] .14 .555 .55 11.37 .97 1779. B6. 1.64 .08 1.72 .00 .97 .885 .57 11.38 1.01 1776. B8. 1.69 .08 1.78 .00 1.91 1.595 .60 11.40 1.06 1771. 93. 1.78 .05 1.88 .00 4.16 1.555 .59 11.39 1.04 1773. 91. 1.75 .09 1.84 .00 .92 .970 .65 11.43 1.15 1764. 100. 1.91 .11 2.02 .00 .10 .910 .67 11.44 1.18 1762. 103. 1.96 .11 2.08 .00 6.84 .550 .67 11.44 1.19 1761. 104. 1.98 .12 2.10 .00
     MALL FLUID REYNOLDS PRANDTL Toulk/ MUDulk/ NUSSELT STANTON
     LOC. VEL. NUMBER NUMBER Twall MUwall NUMBER NUMBER
.14 351.4 .1509E+07 1.215 .662 1.80 .1833E+04 .9994E-03 .97 357.4 .1460E+07 1.315 .652 1.97 .1852E+04 .9646E-03 1.91 369.0 .1530E+07 1.296 .638 2.00 .1810E+04 .9125E-03 4.16 385.3 .1641E+07 1.297 .679 1.85 .2172E+04 .1021E-02 5.02 400.3 .1743E+07 1.306 .635 1.84 .1993E+04 .8754E-03 6.84 424.3 .1903E+07 1.312 .633 1.76 .2064E+04 .8602E-03 6.84 424.3 .1903E+07 1.314 .639 1.71 .2165E+04 .8654E-03
WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY LOC. TEMP. PRESS VISCOSITY CONDUCTIVITY HEAT
CALC. CHECK: Wattmeter De =14.13[kw] Sensible Ds =14.82[kw] Gerr = 4.89%
CALC. CHECK: Wattmeter De =14.13[kw] Sensible Ds =14.82[kw] Ger

Meas. V = 7.607 [volts] Calc. V = 7.575 [volts] Verr = .413%

Meas. I =1856.9 [amps] Calc. I =1864.6 [amps] Jerr = .41%

Meas. Tout = -41.7 [F] Calc. Tout = -45.0 [F] Terr = 3.3 [F]
```

)

OF POOR QUALITY METHANE HEAT TRANSFER INVESTIGATION CASE = 5-18-48 TIME = 15:39:27 # DF TC = 7 TUBE L = 7.02 [in] $(Q_{abse} = 18.38 \text{ [KWe]} = 1 = 2008.6 \text{ [emps]} V = 9.148 \text{ [volts]} R = 4.55 \text{ [mOhms]}$ T u/s=-112.6 [F] T d/s= -19.2 [F] Pin =4443.0 [psia] Pout = 3569.0 [psia] T in = -115.8 [F]Tout = -26.1 [F] H in= 256.9 H out = 336.6 [Btu/1b] Vol Flow = 4.63 [GPM] Mass Flow = .2240[1b/s] Mass Flux = 53.52[1b/s-in2] WALL X/ID DUTER INTERF INNER FLUID ADIF . FLUID HEAT h TRANSFER LOC. Wall Wall 1all Bulk WALL T PRESS FLUX COEFFICIENT X[in] [[in] T[F] T[F] T[F] T[F] [psia] [Btu/s-in**2]
.14 1.9 122.6 114.6 110.2 -112.5 -109.2 4007.6 9.410 .42894E-01 .14 1.9 122.6 114.6 110.2 -112.5 -109.2 4007.6 9.410 .42894E-01 .97 13.3 149.8 141.3 136.6 -104.0 -100.4 3969.9 9.825 .41444E-01 1.91 26.2 198.2 188.7 183.7 -88.5 -84.7 3899.6 10.559 .39340E-01 4.16 57.0 180.8 171.7 166.8 -68.8 -64.7 3806.0 10.299 .44498E-01 5.02 68.8 271.0 260.1 254.5 -52.8 -48.3 3726.2 11.658 .38496E-01 6.10 83.6 303.3 291.8 285.9 -40.0 -35.2 3662.0 12.138 .37799E-01 6.84 93.7 319.5 307.7 301.7 -30.0 -24.8 3609.7 12.380 .37919E-01

WALL	TUBE	RESISTANCE	VOLTAGE	CUR	RENT	HEAT	GEN.	TOTAL	HEAT
LOC.	S EG DL	CU MONE	L	CU	MONEL	CU	MONEL	Q GEN	LOSS
X[in]	[in]	[mDhms/in]	[volt/in	3 Cam	ps]	[Btu	/s-in]	[Btu/s	
.14	. 5 55	.59 11.4	0 1.13	1909.	9 9.	2.05	.11	2.16	.00
.9 7	. 8 85	.62 11.4	1 1.18	1905.	104.	2.14	.12	2.25	.00
1.91	1.595	.67 11.4	4 1.27	1897.	111.	2.29	.13	2.42	.00
4.16	1.555	.65 11.4	3 1.24	1900.	109.	2.23	.13	2.36	.00
(02	.970	.74 11.4	9 1.40	1886.	122.	2.51	. 16	2.67	.00
\.10	.910	.78 11.5	1 1.46	1881.	127.	2.61	.18	2.78	.00
6.84	. 55 0	.79 11.5	2 1.49	1879.	130.	2.66	.18	2.B4	.00

WALL LOC. X[in]	FLUID VEL. [ft/s]	REYNOLDS NUMBER	PRANDTL NUMBER	Tbulk/ Twall	MUbulk/ MUwall	NUSSELT NUMBER	STANTON NUMBER
.14	360.0		1.210	. 609	2.00	.1822E+04	.9693E-03
.9 7		. 150BE+07	1.311	.597	2.12	.1841E+04	.9313E-03
1.91	382.9	.1611E+07	1.294	.577	2.01	.1818E+04	.8719E-03
4.16	405.0	.1762E+07	1.304	.624	1.86	.2217E+04	.964BE-03
5.02	426.1	.1902E+07	1.314	.570	1.76	.2045E+04	.8185E-03
6.10	445.2	.2027E+07	1.315	.563	1.67	.2112E+04	.7924E-03
6.84	461.8	.21337+07	1.311	. 565	1.59	.2201E+04	.7871E-03

WALL LOC.	FLUID TEMP.	FLUID PRESS	ENTHALPY	DYNAMIC VISCOSITY	THERMAL CONDUCTIVITY	SPECIFIC HEAT	DENSITY
XEin3	(F) -112.5	[psia]		[lb/ft-s]	[Btu/s-ft]	[Btu/1b-R]	
. 97	-104.0	4007.6 3969.9		.3019E-04 .3110E-04	.20626E-04 .19721E-04	.8268 .8315	21.409
1.91 4.16	-8 8.5 -68.8	3 899.6 3806.0		.2910E-04	.18956E-04 .17584E-04	.8431 .8618	20.129 19.028
5.02	-52.8 -40.0	3726.2 3662.0	310.591	.2464E-04	.16487E-04	. 8788	18.085
B4	-30.0	3609.7		.2313E-04 .2198E-04	.1567BE-04 .150B9E-04	. 9 913 . 9 001	17.310 16.688

CALC. CHECK: Wattmeter Ge =18.38[kw] Sensible Qs =18.85[kw] Gerr = 2.59%

on your thank on a contribution of an anaparagement of the contribution of the contrib

Meas. V = 9.168 [volts] Calc. V = 9.148 [volts] Verr = .22% Meas. I =2004.2 [amps] Calc. I =2008.6 [amps] Ierr = .22% Meas. Tout = -23.9 [F] Calc. Tout = -26.1 [F] Terr = 2.2 [F] Terr = 2.2 [F]

when the second second

HILL STATE OF THE PARTY.

wash abland the area

Ĭ.

٠ 📆 -

Of him is given in

```
CASE = 5-21-1A
                                  TIME = 10:45:08 TUBE L = 7.02 [in] # OF TC = 7
      Vol. Flow = 5.31 [GPM] Mass Flow = .2628[1b/s] Mass Flux = 62.79[1b/s-in2]
     WALL TUBE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT
     LOC. SEG DL CU MONEL CU MONEL Q GEN LOSS
    LDC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [mOhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] .14 .555 .51 11.34 .92 1805. 81. 1.57 .07 1.64 .00 .97 .885 .52 11.35 .94 1804. 82. 1.60 .07 1.67 .00 1.91 1.595 .54 11.36 .98 1800. 86. 1.67 .08 1.75 .00 4.16 1.555 .54 11.36 .96 1801. 85. 1.65 .08 1.73 .00 (92 .970 .58 11.39 1.05 1794. 92. 1.78 .09 1.87 .00 .10 .910 .60 11.39 1.07 1793. 94. 1.81 .09 1.91 .00 6.84 .550 .61 11.40 1.09 1791. 95. 1.84 .10 1.94 .00
    WALL FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON
LOC. VEL. NUMBER NUMBER Twall MUWall NUMBER NUMBER
X[in] [ft/s]
   WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY LOC. TEMP. PRESS VISCOSITY CONDUCTIVITY HEAT X[in] [F] [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3] .14 -125.5 3843.9 248.322 .3246E-04 .20835E-04 .8280 21.908 .97 -120.0 3797.7 252.879 .3127E-04 .20474E-04 .8315 21.603 1.91 -110.2 3712.8 261.021 .2887E-04 .1986BE-04 .8395 21.044 4.16 -98.0 3601.5 271.473 .2899E-04 .18711E-04 .8525 20.305 5.02 -88.1 3508.7 280.074 .2740E-04 .17935E-04 .8658 19.679 10 -80.5 3436.7 286.849 .2618E-04 .17281E-04 .8772 19.177 84 -74.5 3379.4 292.203 .2524E-04 .16760E-04 .8875 18.772
     CALC. CHECK: Wattmeter De =13.18[kw] Sensible Os =15.23[kw] Gerr = 15.57%
```

```
ORIGINAL PAGE 10
                         METHANE HEAT TRANSFER INVESTIGATION
                                                                       OF POOR QUALITY
  CASE = 5-21-1B
                      TIME = 10:46:34
                                               TUBE L = 7.00 [in]
                                                                         # OF TC =
  (Obbse =19.73 [KWe] I =2077.9 [amps] V = 9.492 [volts] R = 4.57 [mDhms]
  T u/s=-117.5 [F] T d/s= -22.2 [F] Pin =4395.0 [psia] Pout = 3432.0 [psia]
                        Tout = -33.0 [F] H in= 252.1
                                                                     H out = 334.2 [Btu/16]
  Vol Flow = 4.96 [GPM]
                               Mass Flow = .2423[1b/s] Mass Flux = 57.89[1b/s-in2]
  WALL X/ID OUTER INTERF INNER FLUID ADIAB. FLUID
                                                                    HEAT
  LOC.
                                                                            h TRANSFER
                        WALL WALL
                WALL
                                                WALL T PRESS FLUX
                                        BULK
 XCin3
                                                                            COEFFICIENT
                TIFI
                        TIF) TIF)
                                        T(F)
                                                T[F] [psia]
 .14 1.9 124.0
                                                                   [Btu/s-in+#2]
                       115.4 110.7 -118.0 -114.1 3890.4 10.062 .44754E-01
   . 97
        13.3 150.B
                       141.7 136.8 -109.5 -105.4 3847.2 10.498
  1.91
       26.2 198.9 188.8 183.5 -94.2 -89.9 3766.3 11.279 .41261E-01
 4.16 57.0 185.4 175.6 170.4 -75.0 -70.2 3658.3 11.062 .45979E-01 5.02 68.8 280.3 268.5 262.5 -59.3 -54.1 3566.1 12.585 .39754E-01 6.10 83.6 318.1 305.6 299.2 -46.6 -41.0 3491.5 13.184 .38750E-01 6.84 93.7 348.8 335.6 329.0 -36.7 -30.7 3431.3 13.670 .37999E-01
 WALL
         TUBE
                  RESISTANCE VOLTAGE
                                            CURRENT HEAT GEN.
                                                                        TOTAL
 LOC.
        SEG DL
                                                                                 HEAT
                CU MONEL
                                           CU MONEL CU MONEL
                                                                      @ GEN
 X[in] [in]
                [mOhms/in] [volt/in] [amps] [Btu/s-in]
                                                                                 LOSS
 . 14
                                                                       [Btu/s-in]
        . 555
                  .59 11.40 1.17 1975. 103. 2.19 .11
       .885 .62 11.41 1.22 1971. 107. 2.28 .12 2.41 1.595 .67 11.44 1.31 1963. 115. 2.44 .14 2.59 .970 .75 11.49 1.47 1950. 128. 2.71 .18 2.89 .910 .79 11.51 1.54 1945. 133. 2.83 .19 3.02 .530 .82 11.53 1.59 1940. 138. 2.93 .21 3.13
  . 97
                                                                         2.31
1.91
                                                                                 .00
 4.16 1.555
                                                                                 .00
• 22
                                                                                .00
                                                                                .00
⊾.10
6.84
                                                                                  .00
                                                                         3.13
                                                                                  .00
```

İ

uji uji n

1

Land Market

The state of the state of the state of

.

在 村上 一大

٠٠ ا<u>يو</u> ي

WALL LOC. X[in]	- · - ·	REYNOLDS NUMBER	PRANDTL NUMBER	Tbulk/ Twall	MUbulk/ MUwall	NUSSELT NUMBER	STANTON NUMBER
.14 .97 1.91 4.16 5.02 6.10 6.84	394.6 410.9 435.1 458.3 479.4	.1628E+07 .1619E+07 .1737E+07 .1908E+07 .2070E+07 .2214E+07	1.255 1.332 1.307 1.315 1.327 1.334 1.336	.599 .587 .568 .611 .555 .544	2.09 2.16 2.05 1.89 1.78 1.68 1.59	.1905E+04 .1936E+04 .1912E+04 .2298E+04 .2126E+04 .2190E+04	.9324E-03 .8979E-03 .8424E-03 .9159E-03 .7741E-03 .7419E-03

```
WALL FLUID FLUID
                           ENTHALPY DYNAMIC
                                                    THERMAL.
                                                                  SPECIFIC DENSITY
LOC.
        TEMP. PRESS
                                      VISCOSITY CONDUCTIVITY HEAT
X[in] [F]
                [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3]
.14 -118.0 3890.4
                          254.746 .3115E-04 .20581E-04 .8290
 .97 -109.5 3847.2 261.803 .3132E-04 .19618E-04 .8339
       -94.2 3766.3 274.679 .2919E-04 .18904E-04 .8460
1.91
                                                                               21.128
4.16 -75.0 3658.3 291.379 .2657E-04 .17525E-04 .8671
5.02 -59.3 3566.1 305.335 .2450E-04 .16379E-04 .8870
10 -46.6 3491.5 316.781 .2291E-04 .15500E-04 .9022
84 -36.7 3431.3 325.879 .2171E-04 .14834E-04 .9130
                                                                               20.287
                                                                               19.159
                                                                               16.745
```

CALC. CHECK: Wattmeter Ge =19.73[kw] Sensible Gs =20.98[kw] Gerr = 6.37% Meas. V = 9.379 [volts] Calc. V = 9.492 [volts] Verr = 1.212% Meas. I =2103.2 [amps] Calc. I =2077.9 [amps] Ierr = 1.20% Terr = 5.4 [F]

```
METHANE HEAT TRANSFER INVESTIGATION OF PORK CONT.
                                 CASE = 5-21-1C TIME = 10:42:47 TUBE L = 7.02 [in] # OF TC = 7
                           Vol Flow = 3.92 [GPM] Mass Flow = .1714[lb/s] Mass Flux = 40.95[lb/s-in2]
WALL X/ID OUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER LOC. WALL WALL WALL BULK WALL T PRESS FLUX COEFFICIENT TIFJ TIFJ TIFJ TIFJ TIFJ [psia] [Btu/s-in+*2] .14 1.9 23.4 21.0 19.6 -65.9 -63.5 4225.1 2.980 .35846E-01 .97 13.3 27.2 24.8 23.4 -62.5 -60.0 4202.5 3.003 .35999E-01 1.91 26.2 37.6 35.1 33.7 -56.5 -54.0 4161.9 3.064 .34935E-01 4.16 57.0 37.1 34.6 33.2 -49.0 -46.4 4109.4 3.061 .38477E-01 5.02 68.8 54.1 51.5 50.0 -42.9 -40.2 4066.5 3.161 .35041E-01 6.10 83.6 57.9 55.3 53.8 -38.3 -35.5 4033.9 3.184 .35659E-01 6.84 93.7 65.2 62.5 61.0 -34.7 -31.9 4008.3 3.227 .34751E-01
WALL TUBE RESISTANCE CU MONEL 
WALL FLUID REYNOLDS PRANDTL Toulk/ MUDulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUWall NUMBER NUMBER X[in] [ft/s]
WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY VISCOSITY CONDUCTIVITY HEAT SPECIFIC DENSITY CONDUCTIVITY HEAT
```

:

CALC. CHECK: Wattmeter Ge = 5.25[kw] Sensible Os = 5.93[kw] Gerr = 12.96% CALC. CHECK: Wattmeter Qe = 5.25[kw] Sensible Qs = 5.93[kw] Qensible Qs = 5.93[kw] Qs =

The state of the s

And the contract of the con-

```
ORIGINAL Para Con-
                       METHANE HEAT TRANSFER INVESTIGATION OF POOR CONTINUE
    CASE = 5-21-2A
                      TIME = 11:24:51
                                         TUBE L = 7.02 [in]
                                                                 # OF TC =
    (Quber =13.03 [KWe]
                         I =1896.1 [amps] V = 6.869 [volts]
                                                                 R = 3.62 [mDhme]
    T u/s=-125.1 [F]
                     T d/s= -65.3 [F] Pin =4398.0 [psia] Pout = 3244.0 [psia]
    T in =-129.2 [F]
                      Tout = -73.5 [F] H in= 245.3
                                                             H out = 296.0 [Btu/1b]
    Vol Flow = 5.21 [GPM]
                            Mass Flow = .2585[16/s] Mass Flux = 61.76[16/s-in2]
    WALL X/ID OUTER INTERF INNER FLUID ADIAB. FLUID
                                                          HEAT
                                                                   h TRANSFER
    LOC.
                WALL
                      WALL WALL
                                           WALL T PRESS
                                    BULK
                                                           FLUX
    X[in]
                T[F]
                      T(F) T(F)
                                           T(F) [psia]
                                    TLFJ
                                                           [Btu/s-in++2]
    .14 1.9
                 26.8 21.2
                             17.9 -127.0 -122.7 3833.9 7.103 .50506E-01
    .97 13.3 36.1 30.3
                             27.0 -121.4 -117.0 3789.0 7.232
   1.91 26.2 58.9 52.8 49.3 -111.6 -107.1 3706.9 7.548 .48269E-01
4.16 57.0 51.0 45.0 41.6 -99.3 -94.4 3599.2 7.440 .54720E-01
5.02 68.8 95.8 89.0 85.3 -89.4 -84.2 3509.6 8.058 .47531E-01
6.10 83.6 105.9 99.0 95.1 -81.7 -76.3 3440.1 8.198 .47807E-01
    6.84 93.7 118.0 110.9 106.9 -75.7 -70.2 3384.8 8.364
   WALL
          TUBE
                 RESISTANCE VOLTAGE
                                        CURRENT
                                                   HEAT GEN.
                                                               TOTAL
                                                                       HEAT
   LOC.
         SEG DL
                CU MONEL
                                       CU
                                            MONEL CU MONEL Q GEN
                                                                      LOSS
   X[in] [in]
                 [mDhms/in] [volt/in] [amps]
                                                   [Btu/s-in]
                                                               [Btu/s-in]
    . 14
          . 555
                 .50 11.34
                              .91 1B16. BO.
                                                   1.56 .07
                                                                1.63 .00
    . 97
                 .51 11.34
          . 885
                                    1815. 81. 1.59 .07 1.66
1811. 85. 1.65 .08 1.73
1812. 84. 1.63 .08 1.71
                               . 92
   1.91
                                                                       .00
        1.595
                 .53 11.36
                              .96
                                                         .08 1.73
                                                                       .00
   4.16
        1.555
                .52
                      11.35
                                . 95
   ( )2
                                                                       -00
         . 970
                 .57 11.38 1.03
                                     1806. 90. 1.76 .09 1.85
                                                                       .00
         .910
                  . 58
                      11.39 1.05
                                     1804. 92. 1.79 .09 1.88
                                                                       .00
   6.84
          .550
                  .59 11.39
                              1.07
                                            94. 1.82 .09 1.92
                                     1802.
                                                                       .00
        FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON
   WALL
   LOC.
        VEL.
                 NUMBER Twall MUwall
                                                   NUMBER
                                                             NUMBER
   X[in] [ft/s]
    . 14
        404.8 .1655E+07 1.296
                                   .697 1.70
                                                    21105104
```

8

G.

. . .

3

ري وي المحالية والمراجع في المراجع الم

1

Tariffe ...

-

を記す

WALL	FLUID	FLUID	ENTHALPY	DYNAMIC	THER	MAL SPECI	FIC DENSITY	,
5.02 6.10 6.84	450.4 462.1	.1964E+ .2054E+ .2130E+	07 1.322 07 1.329		1.73 1.87 1.84 1.82	.2553E+04 .2310E+04 .2414E+04 .2457E+04	.1040E-02 .8900E-03 .8840E-03 .8633E-03	
.97 1.91 4.16	421.3	.1715E+ .1852E+ .1856E+	07 1.231	. 684	1.72 1.74	.2118E+04 .2143E+04 .2124E+04	.9875E-03 .9780E-03 .9314E-03	

LOC. TEMP.	FLUID PRESS	ENTHALPY	DYNAMIC VISCOSITY	THERMAL CONDUCTIVITY	SPECIFIC	DENSITY
X[in] [F] .14 -127.0 .97 -121.4 1.91 -111.6 4.16 -99.3 5.02 -89.4 10 -81.7 .84 -75.7	[psia] 3833.9 3789.0 3706.9	247.026 251.620 259.809 270.318 278.961 285.756	11b/ft-m] .3269E-04 .3154E-04 .2921E-04 .2915E-04 .2756E-04 .2634E-04		[Btu/1b-R] .8281 .8311 .8391 .8518 .8646 .8755	21.974 21.668 21.110 20.372 19.748 19.249
					. 8854	18.847

CALC. CHECK: Wattmeter Be =13.03[kw] Sensible ws =13.03[kw] Meas. V = 6.783 [volts] Calc. V = 6.869 [volts] Verr = 1.274% T =1920.2 [amps] Calc. I =1896.1 [amps] Ierr = 1.26% Terr = 3.2 [f] CALC. CHECK: Wattmeter De =13.03[kw] Sensible Os =13.84[kw] Gerr = 6.25% Terr = 3.2 [F]

The state of the s

```
CASE = 5-21-2B
                                                                           TIME = 11:25:54 TUBE L = 7.02 [in] # OF TC =
  Vol Flow = 5.05 [GPM] Mass Flow = .2489[lb/s] Mass Flux = 59.48[lb/s-in2]
        WALL TUBE RESISTANCE CU MONEL 
       WALL FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUwall NUMBER NUMBER
        X[in] [ft/s]
      .14 393.3 .1630E+07 1.279 .634 1.99 .2043E+04 .9796E-03 .97 400.6 .1718E+07 1.245 .628 1.98 .2049E+04 .9575E-03 1.91 415.1 .1740E+07 1.318 .613 2.09 .2074E+04 .9040E-03 4.16 436.0 .1894E+07 1.316 .657 1.92 .2508E+04 .1006E-02 5.02 455.6 .2037E+07 1.326 .607 1.85 .2298E+04 .8508E-03 6.84 488.0 .2268E+07 1.344 .599 1.70 .2466E+04 .8090E-03
  CALC. CHECK: Wattmeter Ge =17.48[kw] Sensible Qs =17.97[kw] Qerr = 2.82%
```

- The same of the

OF POOL GOLDING METHANE HEAT TRANSFER INVESTIGATION CASE = 5-21-3A TIME = 1:16:40 TUBE L = 7.02 [in] # OF TC = 7 (Pabse =16.75 [KWe] I =2029.1 [amps] V = 8.255 [volts] R = 4.07 [mDhms] T u/s=-118.9 [F] T d/s= -42.2 [F] Pin =4416.0 [psia] Pout = 3273.0 [psia] T in =-123.0 [F] Tout = -52.0 [F] H in= 250.5 H out = 316.4 [Rtu/lb] Vol Flow = 5.23 [GPM] Mass Flow = .2565[1b/s] Mass Flux = 61.29[1b/s-in2] WALL X/ID OUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER LOC.

X[in] T[F] T[F] T[F] T[F] T[F] T[F] [psia] [Btu/s-in+2]

.14 1.9 82.0 74.6 70.5 -120.3 -116.0 3853.6 8.958 .48055E-01

.97 13.3 95.1 87.5 83.2 -113.2 -108.8 3807.4 9.164 .47724E-01

1.91 26.2 128.2 119.9 115.4 -100.8 -96.0 3721.5 9.680 .45794E-01

4.16 57.0 114.1 106.1 101.7 -85.1 -80.0 3607.6 9.463 .52088E-01

5.02 68.8 178.1 168.8 163.9 -72.5 -67.0 3511.8 10.458 .45283E-01

6.10 83.6 197.6 188.0 182.9 -62.6 -56.8 3436.2 10.758 .44883E-01

6.84 93.7 213.5 203.5 198.3 -54.9 -48.8 3375.1 11.003 .44519E-01 WALL TUBE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT LOC. SEG DL CU MONEL CU MONEL CU MONEL CU MONEL Q GEN LOSS [Stu/s-in] [In] [mDhms/in] [volt/in] [amps] [Stu/s-in] [Btu/s-in] [Btu/s-in] .14 .555 .55 11.37 1.07 1935. 94. 1.96 .10 2.05 .00 .191 1.595 .60 11.40 1.15 1928. 101. 2.11 .11 2.22 .00 .191 1.555 .58 11.39 1.13 1930. 99. 2.06 .11 2.17 .00 .4.16 1.555 .58 11.39 1.13 1930. 99. 2.06 .11 2.17 .00 .10 .910 .67 11.44 1.28 1917. 112. 2.33 .14 2.47 .00 6.84 .550 .69 11.45 1.31 1914. 115. 2.38 .14 2.52 .00 WALL FLUID REYNOLDS PRANDTL Toulk/ MUDulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUWall NUMBER NUMBER WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY VISCOSITY CONDUCTIVITY HEAT (Btu/1b-R) [Btu/1b-R] [Btu/1b-R] [Btu/1b-R] [Btu/1b-R] [Ib/ft-S] (Btu/1b-R) [Ib/ft-S] (Btu/1b-R) [Ib/ft-S] (Btu/1b-R) [Ib/ft-S] (Btu/1b-R) (Ib/ft-S] (Ib/ft-S] (Btu/1b-R) (Ib/ft-S] (Btu/1b-R) (Ib/ft-S] (Ib/ft-S) (Ib/

CALC. CHECK: Wattmeter Be =16.75[kw] Sensible Ds =17.84[kw] Derr = 6.49% Meas. V = 8.176 [voltu] Calc. V = 8.255 [volts] Verr = .970% Meas. I =2048.8 [amps] Calc. I =2029.1 [amps] Ierr = .96% Meas. Tout = -47.7 [F] Calc. Tout = -52.0 [F] Terr = 4.3 [F]

The state of the s

ال

```
" CASE = 5-21-3B TIME = 1:17:50
                                                                                                            TUBE L = 7.02 [in] # OF TC = 7
 Quber =23.65 [KWe] I =2165.6 [amps] V = 10.920 [volts] R = 5.04 [mDhms] T u/s=-117.6 [F] T d/s= -8.0 [F] Pin =4364.0 [psia] Pout = 3288.0 [psia] T in =-121.3 [F] Tout = -17.4 [F] H in= 251.9 H out = 347.0 [Btu/lb]
       Vol Flow = 4.98 [GPM] Mass Flow = .2433[lb/s] Mass Flux = 58.13[lb/s-in2]
WALL X/ID DUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER WALL X[in] T[F] T[F] T[F] T[F] T[F] T[F] [psia] [Btu/s-in**2] .14 1.9 164.1 154.0 148.5 -117.6 -113.7 3854.5 11.589 .44186E-01 .97 13.3 199.5 188.6 182.8 -107.9 -103.7 3809.7 12.207 .42595E-01 1.91 26.2 260.7 248.5 242.1 -90.2 -85.8 3724.9 13.274 .40485E-01 4.16 57.0 248.4 236.4 230.2 -67.8 -62.8 3610.2 13.062 .44575E-01 5.02 68.8 370.4 355.7 348.4 -49.4 -43.8 3510.5 15.157 .38646E-01 6.10 83.6 433.5 417.4 409.5 -34.3 -28.2 3427.6 16.226 .37077E-01 6.84 93.7 501.1 483.6 474.9 -22.1 -15.4 3357.7 17.361 .35408E-01
WALL YUBE RESISTANCE CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [mOhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] [Btu/s-in] .14 .555 .63 11.42 1.29 2052.113. 2.52 .14 2.66 .00 .97 .885 .67 11.44 1.36 2046.119. 2.65 .15 2.80 .00 .1.91 1.595 .73 11.48 1.48 2036.129. 2.86 .18 3.04 .00 .4.16 1.555 .72 11.47 1.46 2038.127. 2.82 .18 3.00 .00 .10 .97 .97 .98 11.58 1.69 2019.147. 3.24 .24 3.48 .00 .10 .910 .90 11.58 1.81 2009.157. 3.45 .27 3.72 .00 6.84 .550 .97 11.63 1.94 1999.167. 3.67 .31 3.98 .00
WALL FLUID REYNOLDS PRANDTL Toulk/ MUbulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUwall NUMBER NUMBER
WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY VISCOSITY CONDUCTIVITY MEAT [1b/ft3] .14 -117.6 3854.5 254.946 .3098E-04 .20491E-04 .8303 21.535 .97 -107.9 3809.7 263.075 .3100E-04 .19516E-04 .8361 21.018 .191 -90.2 3724.9 278.131 .2856E-04 .18586E-04 .8511 20.036 .16980E-04 .8766 18.715 .502 -49.4 3510.5 314.251 .2327E-04 .15676E-04 .8987 17.571 .10 -34.3 3427.6 328.090 .2148E-04 .14705E-04 .9143 16.605 .84 -22.1 3357.7 339.545 .2011E-04 .13916E-04 .9259 15.785
     CALC. CHECK: Wattmeter De =23.65[kw] Sensible Ds =24.42[kw] Derr = 3.26%
```

The state of the s

Oxionate, 18

OF POUR QUALITY METHANE HEAT TRANSFER INVESTIGATION CASE = 5-21-4A TIME = 2:07:25 TUBE L = 7.02 [in] # OF TC = (Pabse =19.77 [KWe] I =2151.7 [amps] V = 9.190 [volts] R = 4.27 [mDhms] T u/s=-133.2 [F] T d/s= -45.2 [F] Pin =4347.0 [psia] Pout = 3157.0 [psia] T in =-137.8 [F] Tout = -61.3 [F] H in= 237.7 H out = 314.2 [Btu/lb] H out = 314.2 [Btu/lb]Vol Flow = 5.54 [GPM] Mass Flow = .2789[]b/s] Mass Flux = 66.65[]b/s-in2]WALL X/ID OUTER INTERF INNER FLUID ADIAB. FLUID HEAT H TRANSFER LOC. WALL WALL WALL BULK WALL T PRESS FLUX COEFFICIENT X[in] T[F] T[F] T[F] T[F] T[F] [psia] [Btu/s-in##2] .14 1.9 96.3 B7.8 B3.0 -134.9 -130.0 3699.8 10.266 .48190E-01 .97 13.3 115.3 106.4 101.4 -127.5 -122.4 3646.6 10.599 .47350E-01 1.91 26.2 158.0 148.1 142.8 -114.0 -108.8 3547.6 11.344 .45094E-01 4.16 57.0 141.2 131.7 126.5 -97.2 -91.4 3415.9 11.053 .50722E-01 5.02 68.8 225.2 213.9 207.9 -B3.7 -77.4 3304.0 12.505 .43819E-01 6.10 B3.6 253.0 241.1 234.9 -73.0 -66.3 3214.2 12.979 .430B7E-01 6.84 93.7 283.4 270.8 264.3 -64.5 -57.6 3141.0 13.497 .41931E-01 WALL TUBE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT

LOC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [mOhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in]
.14 .555 .56 11.38 1.15 2050. 101. 2.24 .11 2.35 .00
.97 .895 .58 11.39 1.19 2047. 105. 2.31 .12 2.43 .00
1.91 1.595 .63 11.42 1.28 2040. 112. 2.47 .14 2.60 .00
4.16 1.555 .61 11.41 1.24 2043. 109. 2.41 .13 2.53 .00
(02 .970 .69 11.46 1.41 2029. 123. 2.70 .16 2.87 .00
1.91 .910 .72 11.47 1.46 2024. 127. 2.80 .18 2.98 .00
6.84 .550 .75 11.49 1.52 2020. 132. 2.91 .19 3.10 .00

. .

WALL FLUID REYNOLDS PRANDTL Tbulk/ MUbulk/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUwall NUMBER NUMBER X[in] [ft/s]

WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY LOC. TEMP. PRESS VISCOSITY CONDUCTIVITY HEAT X[in] [F] [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3] .14 -134.9 3699.8 240.092 .3367E-04 .21110E-04 .8306 22.258 .97 -127.5 3646.6 246.303 .3219E-04 .20569E-04 .8349 21.850 1.91 -114.0 3547.6 257.599 .2936E-04 .19654E-04 .8451 21.089 4.16 -97.2 3415.9 272.125 .2817E-04 .18247E-04 .8632 20.070 5.02 -83.7 3304.0 284.286 .2598E-04 .17140E-04 .8856 19.178 10 -73.0 3214.2 294.159 .2430E-04 .16216E-04 .9064 18.431 84 -64.5 3141.0 302.091 .2301E-04 .15502E-04 .9242 17.811

CALC. CHECK: Nattmeter De =19.77[kw] Bensible Ds =22.50[kw] Derr = 13.79% Meas. V = 9.130 [volts] Calc. V = 9.190 [volts] Verr = .658% Meas. I =2165.9 [amps] Calc. I =2151.7 [amps] Ierr = .66% Meas. Tout = -51.5 [F] Calc. Tout = -61.3 [F] Terr = 9.8 [F]

the state of the s

METHANE HEAT TRANSFER INVESTIGATION OF FULL CALLS. CASE = 5-21-48.1 TIME = 2:08:29 TUBE L = 7.02 [in] # OF TC = (Qabse =25.52 [KWe] I =2218.1 [amps] V = 11.50B [volts] R = 5.19 [mOhms] T u/s=-127.8 [F] T d/s= -15.6 [F] Pin =4157.0 [psia] Pout = 3094.0 [psia] T in = -131.6 [F]Tout = -25.1 [F] H in= 242.8 H out = 342.0 [Btu/1b] Vol Flow = 5.07 [GPM] Mass Flow = .2515[1b/s]Mass Flux = 60.08[15/s-in2] WALL X/ID DUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER LOC. WALL WALL WALL WALL T BULK PRESS FLUX COEFFICIENT X[in] T[F] TIFI T[F] T[F] TIFI [psia] [Btu/s-in++2] . 14 1.9 160.0 149.6 143.9 -128.0 -123.9 3620.1 12.050 .45002E-01 . 97 13.3 203.3 191.9 185.8 -118.2 -113.9 3573.0 12.846 .42862E-01 1.91 26.2 272.3 259.3 252.5 -100.2 -95.6 14.099 3483.5 .40507E-01 263.3 4.16 57.0 250.5 243.B -77.4 -72.2 3361.5 13.937 5.02 68.B 407.7 391.5 383.4 -58.7 -52.9 3254.1 16.523 .3786BE-01 6.10 **B**3.6 490.4 472.3 463.4 -43.1 -36.6 3162.6 17.979 .35955E-01 93.7 594.3 573.9 563.9 -30.2 -23.1 6.84 30B4.1 19.786

~å }_

The second of the second secon

2

大人 生 一

7.1

WAL		RESISTANCE	VOLTAGE	CUR	RENT	HEAT	GEN.	TOTAL	HEAT
LOC	·	CU MONE	L	CU	MONEL	CU	MONEL	Q GEN	LOSS
XLi		[mDhms/in]	[volt/in] [am	ps]	[Btu	/s-in]	[Btu/s	
. 1		.63 11.4	2 1.31	2103.	115.	2.62		2.76	.00
. 9		.67 11.4	4 1.40	2096.	122.	2.78	. 16	2.95	.00
1.9		.74 11.4		2084.	134.	3.04	.20	3.23	.00
4.1		.73 11.4		2086.	132.	3.01	.19	3.20	.00
()		.87 11.5		2062.	156.	3.52	.27	3.79	.00
L.1		.96 11.6	2 1.96	2049.	169.	3.81	.31	4.12	.00
6.8	4 .550	1.06 11.6	B 2.16	2033.	185.	4.16	.38	4.54	.00

WALL LOC. X[in]	FLUID VEL. [ft/s]	REYNOLDS NUMBER	PRANDTL NUMBER	Tbulk/ Twall	MUbulk/ MUwall	NUSSELT NUMBER	STANTON NUMBER
. 14		.1635E+07	1.309	.550	2.30	.1918E+04	.8961E-03
. 97		.173BE+07	1.280	.529	2.1B	.1885E+04	.8473E-03
1.91	426.1	-1826E+07	1.330	.505	2.11	.1910E+04	.7864E-03
4.16		.2064E+07	1.337	.544	1.89	. 2286E+04	.B2B0E-03
5.02	489.9	-2294E+07	1.361	.476	1.65	.2145E+04	.6871E-03
6.10	522.4	.2509E+07	1.377	.452	1.47	.2195E+04	.6352E-03
6.84	553.8	.2703E+07	1.386	.420	1.32	.2192E+04	.5849E-03

WALL LOC.	FLUID TEMP.	FLUID PRESS	ENTHALPY	VISCOSITY	THERMAL CONDUCTIVITY	SPECIFIC HEAT	DENSITY
X[in]		[psia]		[lb/ft-s]	[Btu/s-ft]	[Btu/1b-R]	[1b/ft3]
	-128.0	3620.1	245.824	.3219E-04	.20549E-04	.8359	21.855
	-118.2	3573.0	254.0 B4	.302BE-04	.19919E-04	.8420	21.323
	-100.2	3483.5	269.510	.28B2E-04	.18580E-04	.8574	20.302
	-77.4	3361.5	289.673	.2550E-04	.16900E-04	.8864	18.910
5.02	-58.7	3254.1	306.942	.2294E-04	.15463E-04	.9174	17.560
10	-43.1	3162.6	321.675	.2097E-04	.14352E-04	.9421	16.562
84	-30.2	3084.1	334.054	.1947E-04	.13473E-04	.9592	15.622

CALC. CHECK: Wattmeter De =25.52[kw] Sensible Os =26.31[kw] Qerr = Meas. V =11.225 [volts] Calc. V =11.508 [volts] Verr = 2.518% Meas. I =2273.9 [amps] Calc. I =2218.1 [amps] Ierr = 2.46% Meas. Tout = -22.0 [F] Calc. Tout = -25.1 [F]

φ 0

```
CASE = 5-21-48.2 TIME = 2:08:35 TUBE L = 7.02 [in] # OF TC = 7
Gubse =25.35 [KWe] I =2208.1 [amps] V = 11.481 [volts] R = 5.20 [: Ohms] T u/s=-126.7 [F] T d/s= -13.2 [F] Pin =4126.0 [psia] Pout = 3019.0 [psia] T in =-130.7 [F] Tout = -27.1 [F] H in= 243.5 H out = 344.6 [Btu/lb]
     Vol Flow = 5.17 [GPM] Mass Flow = .2552[1b/s] Mass Flux = 60.96[1b/s-in2]
 WALL X/ID OUTER INTERF INNER FLUID ADIAB. FLUID HEAT & TRANSFER
   WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY VISCOSITY CONDUCTIVITY HEAT

X[in] [F] [psia] [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3]

.14 -127.1 3571.6 246.493 .3190E-04 .20407E-04 .8380 21.773

.97 -117.5 3523.3 254.605 .3000E-04 .19778E-04 .8444 21.245

1.91 -100.0 3431.2 269.713 .2859E-04 .18444E-04 .8603 20.235

4.16 -77.8 3305.6 289.524 .2528E-04 .16760E-04 .8914 18.847

5.02 -59.5 3195.0 306.408 .2274E-04 .15354E-04 .9237 17.608

10 -44.4 3100.9 320.786 .2080E-04 .14249E-04 .9493 16.519

84 -32.0 3020.3 332.834 .1931E-04 .13369E-04 .9669 15.588
   CALC. CHECK: Wattmeter De =25.35[kw] Sensible Qs =27.22[kw] Qerr = 7.36%
   Meas. V =11.225 [volts] Calc. V =11.481 [volts] Verr = 2.278% Meas. I =2258.4 [amps] Calc. I =2208.1 [amps] Ierr = 2.23% Meas. Tout = -19.7 [F] Calc. Tout = -27.1 [F] Terr = 7.4 [F]
```

ر. سند کستند و میدادن استفاصه که درویقی مواده از واقعالی میشود مهمین میدست بسوی میشود. و حافظ می میشود میشود میشود

Distriction of the state of the

ORIGINAL PAGE IS METHANE HEAT TRANSFER INVESTIGATION OF POOR QUALITY CASE = 5-21-40TIME = 2:09:15TUBE L = 7.02 [in] # OF TC = (*O*abse =30.33 [kWe] I =2238.9 [amps] V = 13.544 [volts] R = 6.05 [mOhms] T d/s= 11.2 [F] Fin =3995.0 [psia] Fout = 2855.0 [psia] | u/s=-123.2 [F] T in =-126.8 [F] .5 (F) Tout = H in= 246.6 H out = 368.5 [Btu/16] Vol Flow = 4.96 [GPM] Mass Flow = .2422[1b/s]Mass Flux = 57.86[1b/s-in2] WALL X/ID OUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER LOC. WALL WALL WALL BULK WALL T PRESS FLUX COEFFICIENT X[in] TEFI T[F] T[F] T[F] T[F] [psia] [Btu/s-in**2] .14 1.9 213.8 201.9 195.6 -122.7 -118.8 3488.4 13.270 .97 13.3 279.6 266.2 259.2 -111.5 -107.5 3442.3 14.485 1.91 26.2 380.7 364.9 356.9 -90.6 -86.0 3352.3 16.329 4.16 57.0 420.6 405.9 395.5 -63.2 -57.9 3225.3 17.049 .37601E-01 5.02 634.6 68.8 612.9 602.3 -39.7 -33.6 3107.6 20.846 6.10 83.6 700.4 677.3 666.0 -20.3 -13.03001.8 21.991 .32367E-01 727.5 703.8 692.2 6.84 93.7 -5.1 3.3 2909.7 22.457 .32597E-01 WALL TUBE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT LOC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN X[in] [in] [mOhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] .555 . 14 .68 11.45 1.43 .17 2114. 125. 2.87 3.04 .00 .97 .885 .74 11.49 1.57 2103. 136. 3.12 .20 3.32 .00 1.51 1.595 . 85 11.55 1.76 2086. 153. .26 3.49 3.74 .00 4.16 1.555 .85 11.58 1.84 2080. 159. 3.63 .28 3.91 .00 . 970 02 1.10 (.10 11.71 2.25 2046. 192. 4.37 .41 .00 4.78 .910 1.17 11.75 2.38 2037. 202. 4.59 .46 5.04 .00 6.84 .55. 1.19 11.76 2.43 2033. 206. .47 5.15 4.66 .00

The second

.

والمارية المراجع المرا

とうないのはないない

7 m.

1

1

S. Salara

7-7

WALL LOC. X[in]	FLUID VEL. [ft/s]	REYNOLDS NUMBER	PRANDTL NUMBER	Tbulk/ Twall	MUbuli/ MUwall	NUSSELT NUMBER	STANTON NUMBER
.14 .97 1.91 4.16 5.02 6.10	399.4 424.5 466.1 512.8	.1642E+07 .1777E+07 .1874E+07 .2178E+07 .2484E+07 .2770E+07	1.302 1.259 1.336 1.363 1.365 1.399	.514 .485 .452 .464 .396	2.26 2.10 1.95 1.67 1.36 1.20	.1849E+04 .1795E+04 .1825E+04 .2105E+04 .2049E+04	.8649E-03 .8018E-03 .7290E-03 .7093E-03 .5957E-03
6.84		.3012E+07	1.399	. 395	1.09	.2405E+04	.5706E-03

```
WALL FLUID FLUID ENTHALPY DYNAMIC
                                                        SPECIFIC DENSITY
                                             THERMAL
    LOC. TEMP.
               PRESS
                                  VISCOSITY CONDUCTIVITY
                                                          HEAT
    X[in] [F]
                 [psia]
                       [Btu/lb] [lb/ft-s] [Btu/s-ft] [Btu/lb-R] [lb/ft3]
    .14 -122.7
                3488.4
                         250.095 .3087E-04 .19993E-04
                                                        .8433
     .97 -111.5
                3442.3
                         259.693 .2852E-04
                                            .19284E-04
                                                         .8514
    1.91
         -90.6
                 3352.3
                         278.051 .2705E-04
                                            .17692E-04
                                                         .8739
   4.16
          -63.2
                 3225.3
                         302.976 .232BE-04
                                            .1564BE-04
                                                         .9162
                                                                  17.876
    5.02
          -39.7
                3107.6
                         325.103 .2040E-04
                                            .14015E-Q4
                                                         .9511
    4.10
         -20.3
                          343.955 .1830E-04
                3001.B
                                            .12767E-04
                                                         .9759
                                                                  14.631
🈘 ( .84
          -5.1
                 2909.7
                         359.444 .1683E-04
                                            .11875E-04
                                                         .9873
```

CALC. CHECK: Wattmeter Qe =30.33[kw] Sensible Qs =31.14[kw] Qerr = 2.70% Verr =18.067%) mit ; range Meas. V =11.472 [volts] Calc. V =13.544 [volts] Meas. I =2643.5 [amps] Calc. 1 =2238.9 [amps] lerr = 15.30% / Meas. Tout = 3.7 [F] Calc. Tout = .5 (F) Terr = 3.2 (F)

want work the server - - myselfer - of the source of the source

Marine - Angele Company and Co

Chickey . METHANE HEAT TRANSFER INVESTIGATION OF Pi CASE = 5-24-2A TIME = 11:00:48 TUBE L = 7.02 [in] # OF TC = Qabse =35.67 [KWe] I =2442.4 [amps] V = 14.607 [volts] R = 5.98 [mDhms] I u/s=-120.3 [F] T d/s= 6.7 [F] Pin =4380.0 [psia] Pout = 2477.0 [psia] T in =-125.5 [F] Tout = -.4 [F] H in= 248.0 H out = 362.0 [Btu/1b] Vol Flow = 5.87 [GPM] Mass Flow = .2881[1b/s] Mass Flux = 68.84[1b/s-in2] TUBE RESISTANCE VOLTAGE CURRENT HEAT GEN. TOTAL HEAT SEG DL CU MONEL CU MONEL Q GEN LOSS WALL LOC. SEG DL CU MONEL LOC. SEG DL CU MONEL CU MONEL CU MONEL Q GEN LOSS X[in] [in] [in] [mOhms/in] [volt/in] [amps] [Btu/s-in] [Btu/s-in] .14 .555 .73 11.49 1.68 2296. 146. 3.66 .23 3.89 .00 .97 .885 .81 11.54 1.85 2282. 161. 4.01 .28 4.29 .00 1.91 1.595 .88 11.58 2.01 2269. 173. 4.32 .33 4.65 .00 4.16 1.555 .95 11.62 2.14 2258. 184. 4.58 .37 4.95 .00 (.02 .970 1.01 11.66 2.26 2248. 194. 4.82 .42 5.23 .00 (.10 .910 1.00 11.65 2.25 2250. 193. 4.79 .41 5.20 .00 6.84 .550 1.03 11.67 2.30 2245. 197. 4.90 .43 5.33 .00 WALL FLUID REYNOLDS PRANDTL TOULK/ MUDULK/ NUSSELT STANTON LOC. VEL. NUMBER NUMBER Twall MUWall NUMBER NUMBER

WALL FLUID FLUID ENTHALPY DYNAMIC THERMAL SPECIFIC DENSITY VISCOSITY CONDUCTIVITY HEAT [16.7] [F] [psia] [Btu/1b] [1b/ft-s] [Btu/s-ft] [Btu/1b-R] [1b/ft3] .14 -121.0 3670.9 251.799 .3112E-04 .20267E-04 .8364 21.552 .97 -108.8 3606.2 262.157 .3041E-04 .19173E-04 .8453 20.872 1.91 -86.4 3478.5 281.551 .2708E-04 .17755E-04 .8689 19.556 4.16 -57.5 3296.0 307.788 .2303E-04 .15513E-04 .9135 17.671 5.02 -34.3 3126.9 330.009 .2002E-04 .13800E-04 .9519 15.964 .10 -17.4 2979.1 346.851 .1799E-04 .12576E-04 .9811 14.610 84 -5.0 2851.6 360.397 .1657E-04 .11701E-04 .9946 13.533

CALC. CHECK: Wattmeter De =35.67[kw] Sensible Ds =34.65[kw] Derr = 2.86% Meas. V =14.659 [volts] Calc. V =14.607 [volts] Verr = .353% Meas. I =2433.7 [amps] Calc. I =2442.4 [amps] lerr = .36% Meas. Tout = -4.1 [F] Calc. Tout = -.4 [F] Terr = 3.7 [F]

Willell The Control of the Control

word of a comment of the state
CASE = 5-24-2BTIME = 11:01:28TUBE L = 7.02 [in] # OF TC = 7 (Qabse =39.92 [KWe] I =2473.8 [amps] V = 16.139 [volts] R = 6.52 [mDhms] T u/s=-116.5 [F] T d/s= 24.1 [F] Pin =4375.0 [psia] Pout = 2421.0 [psia] T in = -121.4 [F]Tout = 22.8 [F] H in= 251.6 H out = 377.3 [Btu/1b] Vol Flow = 5.71 [GPM] Mass Flow = .2780[1b/s] Mass Flux = 66.43[1b/s-in2]

WALL X/ID DUTER INTERF INNER FLUID ADIAB. FLUID HEAT h TRANSFER LDC. WALL WALL WALL BUL! WALL T PRESS FLUX COEFFICIENT X[in] T[F] T[F] T[F] T[F] T[F] [psia] [Btu/s-in##2] . 14 1.9 324.2 306.9 298.0 -116.4 -111.2 3708.6 18.453 .45092E-01 .97 13.3 432.4 422.0 -102.3 -96.7 453.3 3644.9 21.271 1.91 26.2 549.1 .41015E-01 525.6 513.9 -75.8 -69.5 3516.3 23.329 57.0 4.16 577.8 553.5 541.5 -42.2 -34.5 3328.8 23.939 68.8 637.0 611.1 598.3 -15.8 5.02 -6.3 3151.0 25.193 .41669E-01 83.6 633.6 607.8 595.1 6.10 3.3 14.9 2990.7 25.121 6.84 93.7 666.6 639.9 626.7 17.5 31.5 2848.9 25.816

WALL LOC. X[in]	TURE SEG DL [in] .555	RESISTANCE CU MONEL [mDhms/in]	[volt/in]	CURRENT CU MONEL [amps]	HEAT GEN. CU MONEL [Btu/s-in]	TOTAL HEAT Q GEN LOSS [Btu/s-in]
.97 1.91 4.16	.885 1.595 1.555	.78 11.52 .91 11.60 1.00 11.65 1.03 11.67 1.09 11.71	2.08 2.28 2.34	2317. 157. 2294. 179. 2278. 196. 2273. 201.	3.96 .27 4.52 .35 4.93 .42 5.04 .45	4.23 .00 4.88 .00 5.35 .00 5.49 .00
6.84	.910 .550	1.09 11.71 1.12 11.73	2.46	2263. 210. 2264. 210. 2258. 215.	5.29 .49 5.27 .49 5.41 .52	5.78 .00. 5.76 .00 5.92 .00

WALL LOC. X[in]	FLUID VEL. [ft/s]	REYNOLDS NUMBER	PRANDTL NUMBER	Tbulk/ Twall	MUbulk/ MUwall	NUSSELT NUMBER	STANTON NUMBER
.14 .97 1.91 4.16 5.02 6.10 6.84	465.0 502.8 567.4 640.5 712.4	.1920E+07 .1960E+07 .2236E+07 .2679E+07 .3117E+07 .3490E+07	1.260 1.324 1.327 1.353 1.372 1.372	.453 .406 .394 .417 .420 .439	2.17 2.04 1.75 1.46 1.24 1.12	.1963E+04 .1890E+04 .2039E+04 .2461E+04 .2802E+04 .3213E+04	.8113E-03 .7286E-03 .6872E-03 .6790E-03 .6549E-03

WALL LOC. X[in]	FLUID TEMP.	FLUID PRESS	ENTHALPY	VISCOSITY		SPECIFIC HEAT	DENSITY
.14 -	-116.4	[psia] 3708.6		[1b/ft-s] .3030E-04	[Btu/s-ft] .20121E-04	[Btu/1b-R]	
.97 - 1.91	-102.3 -75.8	3644.9 3516.3	267.797	.2969E-04	.19011E-04	.8367 .8474	21.351 20.572
4.16	-42.2 -15.8	3328.8	321.460	.2603E-04 .2172E-04	•17177E-04 •14792E-04	.8758 .9215	19.027 16.859
4.10	3.3	3151.0 2990.7		.1867E-04 .1667E-04	.13029E-04 .11804E-04	.9578 .9716	14.935
B 4	17.5	2848.9		.1532E-04	.10957E-04	.9626	13.427

CALC. CHECK: Wattmeter Qe =39.92[kw] Sensible Qs =36.90[kw] Qerr = 7.58% Meas. V =16.325 [volts] Calc. V =16.139 [volts] Verr = 1.140% Meas. I =2445.6 [amps] Calc. I =2473.8 [amps] Ierr = 1.15% Meas. Tout = 11.4 [F] Calc. Tout = 22.8 [F] Terr = 11.4 [F]

- The second of
entre of the design of the second of the sec

جهد ومعرف رعمانه فالمعرد مواده بهاده والوالم أرارة المائد المائد والمائد والمائد المائد المائد المائد